

FALL TERM PROJECT



BUMBLE **BEES**

BUMBLE BEES

GROUP #3

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8 DECEMBER 2023

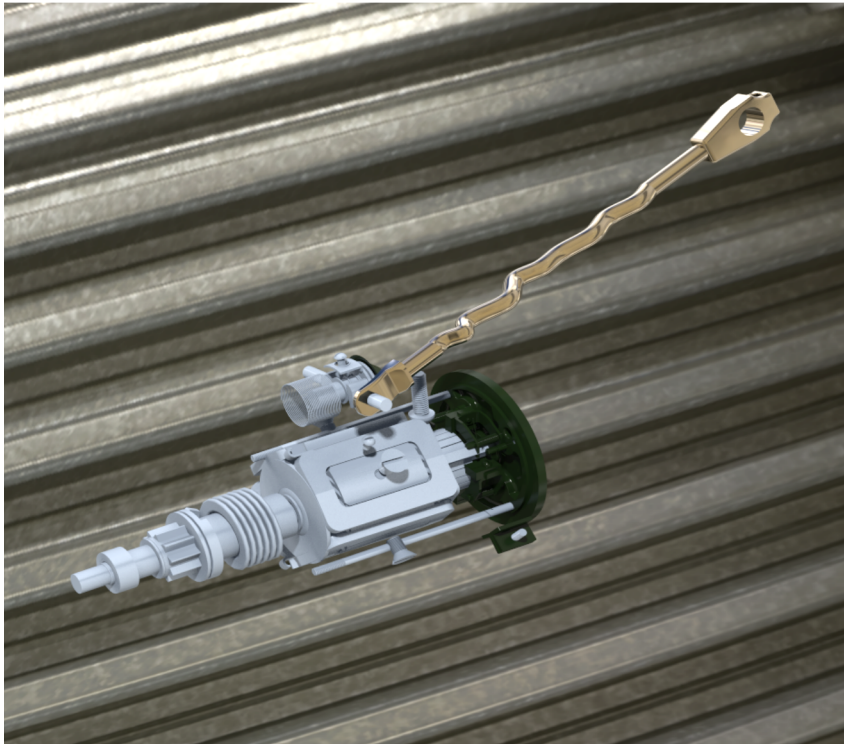
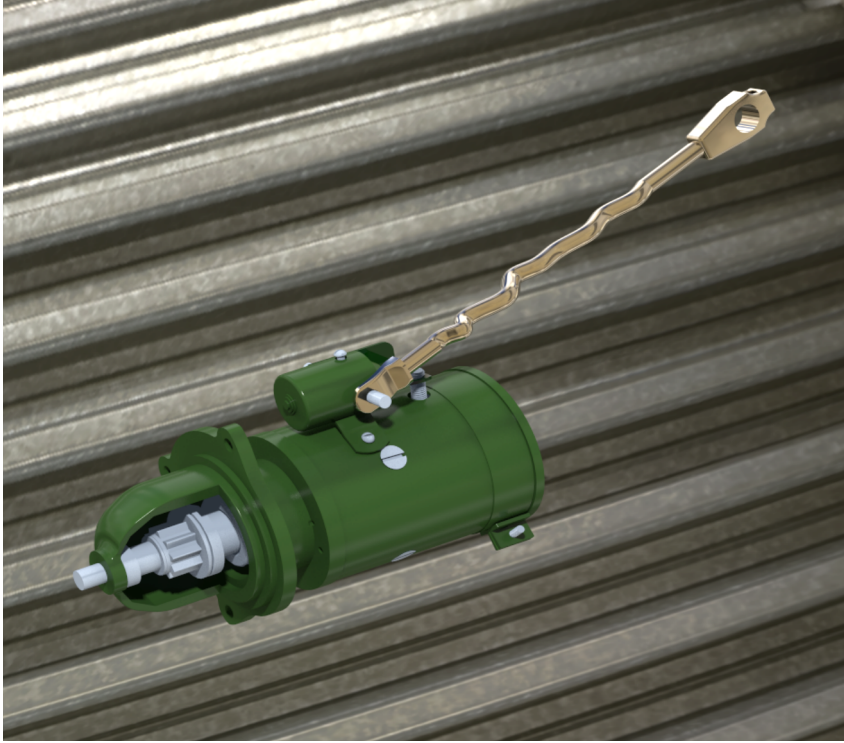
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PROJECT IMAGE



CREO RENDERINGS



INTRODUCTION & HISTORY

Through careful deliberation, the team resolved to disassemble and render a Delco Remy starter, part number 11077424. Though finding information about the basic operations of the starter is painless to find, finding information about our specific part is difficult. No further information can be acquired from the manufacturer's website other than that the part is obsolete, and that it has a sister part, 11074425. Attempts were made to contact the manufacturer, but no further information could be provided. By close inspection of online sources and forums, it can be deduced that the 1945 John B tractor used this starter. It can be reasonably assumed that the part is old, from research collected and the thick layer of rust on the starter.

Before the advent of the starter, a common way to start an engine was the hand-crank method, as seen with the archetypal image of an aviator manually spinning his aircraft's propeller. This however, proved to be inconvenient and dangerous, as the behavior of the engine during start-up was quite unpredictable. A simple violent backfire of the engine could result in broken wrists, fingers, dislocated shoulders, and in the case of bigger engines, fatal injuries. A more convenient fashion to start an engine was necessary. In 1911, Charles Kettering of DELCO invented the electric starter, later used on 1912 Cadillacs. The rest of the industry would follow suit, eliminating the method of hand-cranking.

Coincidentally in 1910, Vincent Bendix almost went bankrupt after the failure of his company. He went back as a car dealer selling Cadillacs in Chicago, right as the electric starter was introduced. Bendix found the mechanism to be complicated and expensive, using a series of solenoids, springs and levers that engaged the starter. Instead, Bendix opted for a triple threaded shaft, where the pinion gear is forced down the shaft's grooves by inertia to mesh with the flywheel. When the engine begins to run under its own power, the high rotation causes the pinion gear to disengage from the flywheel through springs. Starters that did not use this mechanism had to have the gear be engaged and disengaged manually, usually with a pedal. His mechanism saw its first use on the 1914 Cadillac "Baby Grand."

APPLICATIONS

It is difficult to decipher the justification of a starter without first examining the engine as a whole. Thus, to realize the function of a starter, there underlies a necessary discussion of the internal combustion (IC) engine. In the common four-stroke engine system, there are four stages: Intake, Compression, Combustion, and Exhaust. In the intake stroke, the piston moves down inside the cylinder with the concurrent motion of the inlet valve's opening. This creates a vacuum that intakes

the necessary fuel air mixture for later combustion. In newer engines, the inlet valve is replaced by a fuel injection mechanism that injects fuel directly into the cylinder.

As the piston reaches the bottom of its stroke, the fuel intake closes and the piston enters its compression stage. The piston moves upward and compresses the fuel air mixture. As the piston reaches the top of the cylinder the second time, the spark plugs fire, forcing the compressed fuel air mixture to combustion. The force generated by the explosion sends the piston downward, which turns the crankshaft of the engine. As the shaft rotates, the piston rises up again, this time with the concurrent motion of the exhaust valve opening, forcing gasses out and into the exhaust manifold. The rotational action resumes and the piston moves down again, and the process repeats. In order to turn the initial stroke, a high torque mechanism must exist to provide the initial turning of the crankshaft. Thus is the purpose of the starter.

The principal methodology of the starter is to mesh a rotating starter pinion gear to the flywheel in the gearbox housing through extension, thus rotating the crankshaft and overcoming the initial resistance to commence the aforementioned process. Once the engine is running under its own power, the pinion gear is disengaged from the flywheel automatically to prevent backdrive, which is when the engine is driving the starter motor, which can damage both the starter and the engine. This mechanism is typically achieved through an overrunning clutch or a Bendix drive, which employs a series of springs, collars, and rollers to disallow the pinion gear from rotating the rest of the starter motor as the engine begins to run under its own power.

PRODUCT CONSIDERATIONS

With limited knowledge of the specific part the project is applied to, sources of the general nature of starters and their history is relied upon. In general, the weight of the starter, its size, its power output, general material properties, service requirements, and positioning of parts are considered in designing a starter. Different engines may require different starters, as different engines may accommodate differing mounts, orientations, the engine's compression ratio, etc. Starters are typically heavy and made out of steel because if it was too light, it may not have enough structure to turn over the engine. The casing must be strong enough to withstand the high degrees of torque generated by a starter.

The product of this specific project largely mimics the initial form of starters in the early days, excluding the key ignition that largely came about in the 1940s. First, the initial powering of the motor must be considered. To do this, the battery must be connected to the starter motor via a switch. One problem this poses is that the starter motor demands heavy current from the battery, which means the ignition switch and the wires need to be unusually large and bulky.

To circumnavigate this, designers had to consider an external electrical relay, the most common being the solenoid. The power required to supply the starter is first sent through the solenoid by the battery. The solenoid, mounted on the rest of the motor casing (though an external heavy duty electrical relay could be used as an alternative), is an electromagnet that uses small current to energize, which moves a plunger that connects two copper terminals of a contactor switch. A separate connection exists between the battery and the starter motor. When the aforementioned contactor switch is completed, the battery sends electrical current to the starter motor.

A main point of concern is the activation of the pinion gear. One of the main drawbacks of the current configuration of our product is that the pinion gear rotates before it slips into place and mates completely with the flywheel. This method completely relies on the pinion gear being perfectly aligned to the flywheel's gear. Otherwise, the gears clash until both are in a perfect mesh. This leads to greater wear on the gears, requiring higher maintenance in the long run. Over the years, engineers have compensated for this condition by connecting the solenoid plunger to the pinion gear's horizontal movement through an actuating arm. This ensures that the pinion gear is completely meshed with the flywheel before the contactor switch is completed. However, this arm is not present in our current application, and may be a consideration for design change.

Another point of concern is the disengagement of the pinion gear from the flywheel. Normally, the Bendix arrangement allows the pinion to disengage automatically through inertia. As the engine begins to run under its own power, the pinion, meshed with the flywheel, rotates with higher speed and begins to move back into the bendix grooves. As the pinion is still meshed with the flywheel, it may cause a backdrive through the starter motor, which damages it. It also serves the disadvantage in that the pinion may disengage before the engine has the opportunity to start running. Engineers have accounted for this error by using an overrunning clutch, which is a series of springs and rollers that allows the pinion gear to freely roll independent of the starter motor shaft while keeping the pinion engaged.

CALCULATIONS

Part NO.	Part Name	Material	Mass (g)	Volume (cm ³)	CREO Calculated Weight (g)	CREO Calculated Volume (cm ³)
A5	Bolt	Copper	24.50	2.74	25.4	2.84
C1	End Frame	Steel	543.50	68.80	599.3	75.81
C2	Brushes	Copper	11.30	1.26	9.83	1.00
C3	Spring	Copper	2.70	0.30	0.93	0.1
C4	Brush Holder	Copper	7.60	0.85	15.01	1.68
B7	Coil	Steel	224.40	28.41	212	27.12
B9	Pinion	Steel	167.10	21.15	153	19.56
D1	Pole Piece	Iron	168.80	21.45	119.6	17.23
E3	Hoop	Steel	47.90	6.06	21.2	2.72
E1	Drive Housing	Steel	2142.70	271.23	2989	38.17

CONCLUSION

At the conception of the project, 10 parts were selected, at random, to be weighed and have their volumes measured. Once these parts were modeled in CREO, their approximate weights and volumes were calculated by the program, as recorded above. Positioned side by side, it is with much pleasure to say that the majority of the components had their estimated weights and volumes close to the actual measured values. There are a few exceptions, namely part E3. This part was a flexible hoop found in the Solenoid, and the discrepancy of the values could be a product of incorrect material estimation, or a difference in actual material volumes. By parts E1 and C3, divergence from the true values may also be explained by the sheer difficulty of accurately measuring a large, complex structure such as the drive housing, or a small, delicate part such as a spring. Due to the age of our reference part, weather variances may have also impacted the material. It must be noted, that for the majority of our components, a higher volume reflected higher weights for our respective parts, revealing our attention to accuracy to our measurements.

In addition to our consciousness of precision, we were also precise in our progression of the project. In the duration of our endeavor, we hit our deadlines

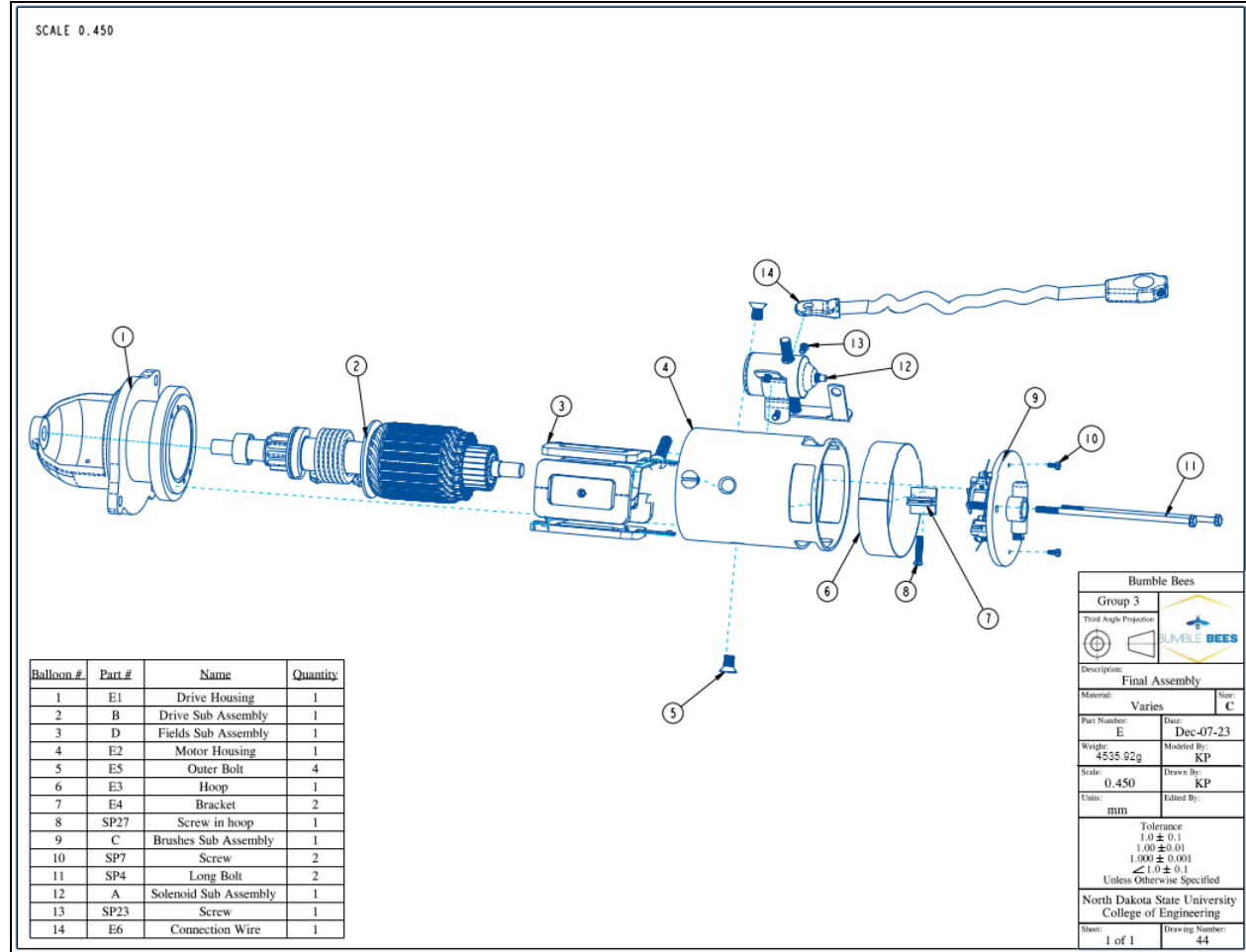
before or on time, and our communication never failed to deliver. Our schedule was structured in a relaxed way, which allowed ample time to focus on each task with detail, disallowed rushed products, all whilst providing adequate time to revise our submissions. Tasks were also satisfied by an even and practical division of labor. For example, parts that were heavily connected together were assigned to the same individual to ensure that the assembly meshed in a more comfortable manner. Given these circumstances, to the highest of our abilities, we were victorious in applying our newly found skills in CREO modeling to deliver a product that we believe to be a success.

BILL OF MATERIALS

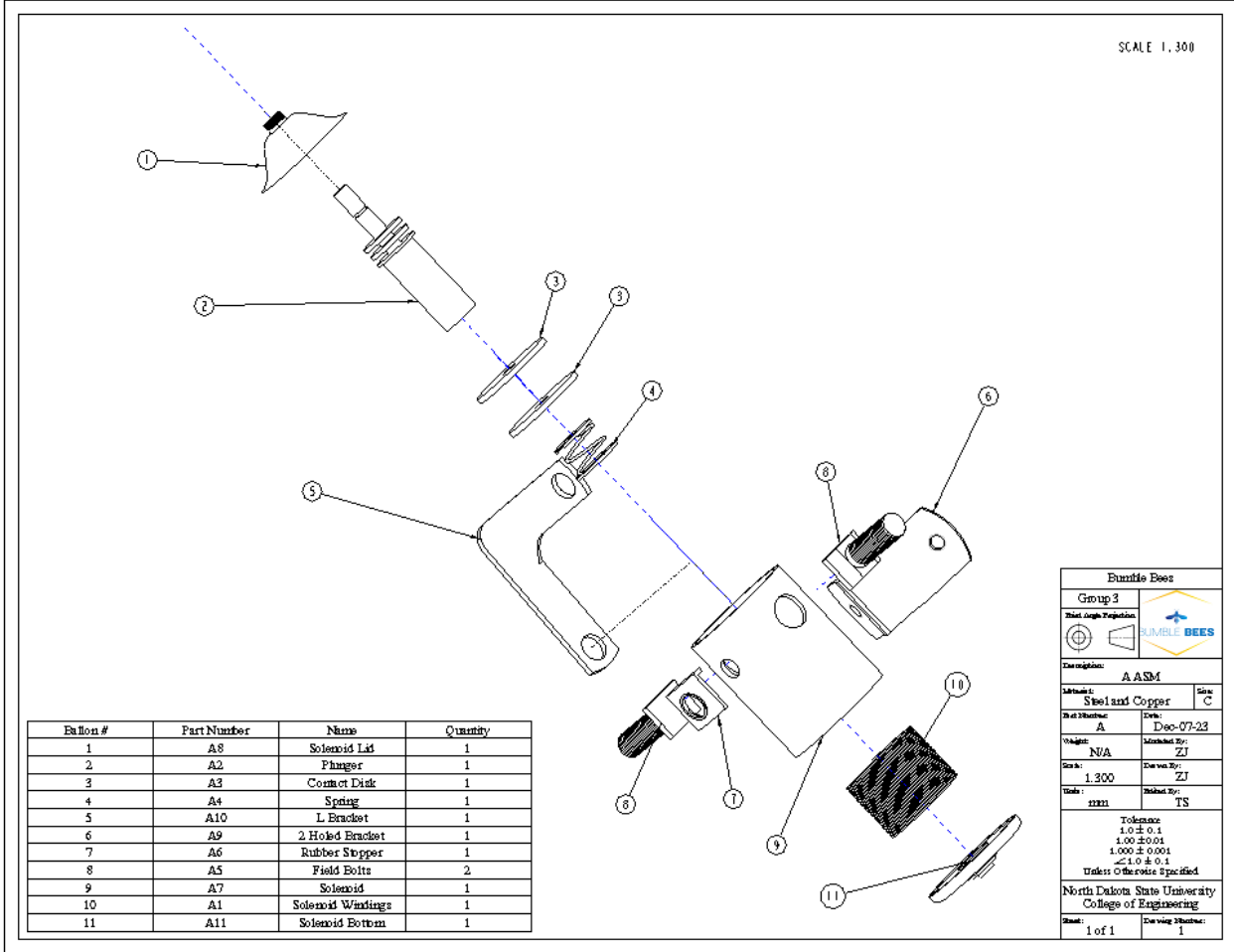
Bill Of Materials					
Levels	Part Number	Drawing Number	Quantity	Part Name	Material
A	A0	1		Solenoid Sub Assembly	
	A1	2	2	Solenoid Windings	Copper
	A2	3	1	Plunger	Iron
	A3	4	2	Contact Disc	Copper
	A4	5	2	Spring	Steel
	A5	6	2	Field Bolts	Copper
	A6	7	1	Rubber Stopper	Rubber
	A7	8	1	Solenoid	Steel
	A8	9	1	Solenoid Lid	Steel
	A9	10	1	2 Holed Bracket	Steel
	A10	11	1	"L" Bracket	steel
	A11	12	1	Solenoid Bottom	steel
B	B0	13		Drive Sub Assembly	
	B2	15	1	Shaft	Steel
	B3	16	1	Commutator	Copper
	B5	18	1	Sleeve Washer	Steel
	B6	19	1	Driving Tail	Steel
	B7	20	1	Driving Head	Steel
	B8	21	1	Multithreaded Sleeve	Steel
	B9	22	1	Coil	Copper
	B10	23	2	Bendix Screw	Steel
	B11	24	1	Pinion	Steel
	B12	25	58	Armature Plate	Steel
	B13	26	1	Pinion Stop	Steel
	B14	27	1	Armature Winds Top	Steel & Copper
	B15	28	23	Armature Insulation Shell	Bakelite
	B16	29	1	Armature Winds Bottom	Steel & Copper
	B18	31	1	Armature Insulation Sheet Btm	Bakelite
	B17	30	2	Armature Insulation Ends	Bakelite
	B18	31	1	Armature Insulation Sheet Top	Bakelite
	B19	32	1	Inside Commutator I	Steel
	B20	51	1	Inside Commutator II	Steel
C	C0	52		Brushes Sub Assembly	
	C1	33	1	End Frame	Steel
	C2	34	4	Brush Holder	Copper
	C3	35	4	Spring	Steel
	C4	36	4	Brushes	Copper
	C5	37	4	Short Wires w/ Brackets	Copper
	C6	38	1	Long Wire w/ Brackets	Copper
	C7	54	1	Small Spring	Steel
D	D0	39		Fields Sub Assembly	
	D1	40	4	Pole Pieces	Iron
	D2	41	1	Right Field Coil	Copper/magnet Wire
	D3	42	1	Left Field Coil	Copper/Magnet Wire
	D4	43	2	Field Coil w/ Hole	Copper/Magnet Wire
E	E0	44		Final Assembly	
	E6	50	1	Connection Wire	Copper
	E5	45	4	Outer Bolt	Steel
	E4	46	2	Bracket	Steel
	E3	47	1	Hoop	Steel
	E2	48	1	Motor Housing	Steel
	E1	49	1	Drive Housing	Steel

Stock Parts			
Part Number	Quantity	Part Name	Ordering Specifics
SP1	2	Washer	16/27 mm
SP2	1	Washer Middle	OD= 25.2, ID= 14.5, 1.8 thick
SP3	3	Washers	9.7/17.5 mm x1 thick
SP4	2	Long Bolt	L=170.4mm, D=5.4mm, Thread L =23mm, Top- 9.5mm L & 4.6mm W
SP5	2	Washer(long bolt)	L=11.7mm, 7.2mm indise, 1.6mm W
SP6	2	Washer	Outside D=11.4mm, Inside D=6.5mm, W=1.7mm M6
SP7	2	Screw	Top D=7.1mm, W=2.5, D=3.6mm, H11.1mm
SP8	2	Washer	In=6.8mm, 4.1mm, W=1.0
SP9	4	Screw	Top D=0.89mm, H=3.6, D=4.6mm, L=9.6mm
SP10	2	Washer	OD=8.3mm, ID=4.9mm, W=1.1mm
SP11	1	Nut	L=9.5mm, W=3.0mm, D=3.5mm
SP12	4	Nut	L=15.7, W=3.9mm, D=8.0mm
SP13	5	Washer	Outside D=16.2mm, Inside D=9.6mm, W=1.6mm
SP14	4	Screw	L=15.0mm, Thread=12.68, D=3.28mm, Top D=6.22
SP15	1	Washer	Outside D= 5.95mm, W=0.8mm, ID=3.6mm
SP16	2	Winged Washer	Outside D=17.5mm, Inside D=9.5mm, Wings- W=4.5mm, H=4.3mm
SP17	3	Rubber Washer	L=19.31mm, D=9.13mm, W=4.45
SP18	1	Washer	L=17.5mm, W=1.7mm, D=9.52mm
SP19	1	Washer	Outside D=17.4, Inside D=9.5mm, W=2.7mm
SP20	3	Rubber Washer	L=17.2mm, Inside D=9.5mm, W=2.7mm
SP21	2	Nut	L15.5mm, inside D=8.0mm, W=6.3mm
SP22	1	Washer	Inside D=20.6mm, Outside D=28.7mm, Thickness=1.5mm
SP23	2	Screw	L=11.3mm, TD=8.6mm, BD=4.6mm
SP24	2	Bolt	L=13.1mm, TD=9.3mm, BD=5.8mm
SP25	1	Bolt	TL=15.7mm, TL=4.5mm, H=22.4mm, BD=9.4mm
SP26	2	Washers	OD=10.0mm, ID=5.5mm, W=1.1mm
SP27	1	Screw in hoop	TD=8.5mm, BD=4.8mm, TH=3mm, H=28.2mm
SP28	1	Screw welded to field coils	TD=16.7mm BD=8.4mm TH=5mm H=40mm
SP29	1	Bolt for Wire	Top=11.8mm x 11.8mm, D=7.0mm, TD=3.7mm, L=40.0mm
SP30	4	Housing Screw	TD=17.5mm BD=9.5mm TH=9.5mm H=16.5mm
SP31	1	Nut(bolt-wire)	OD=13.5mm, ID=7.00mm, D=5.5mm

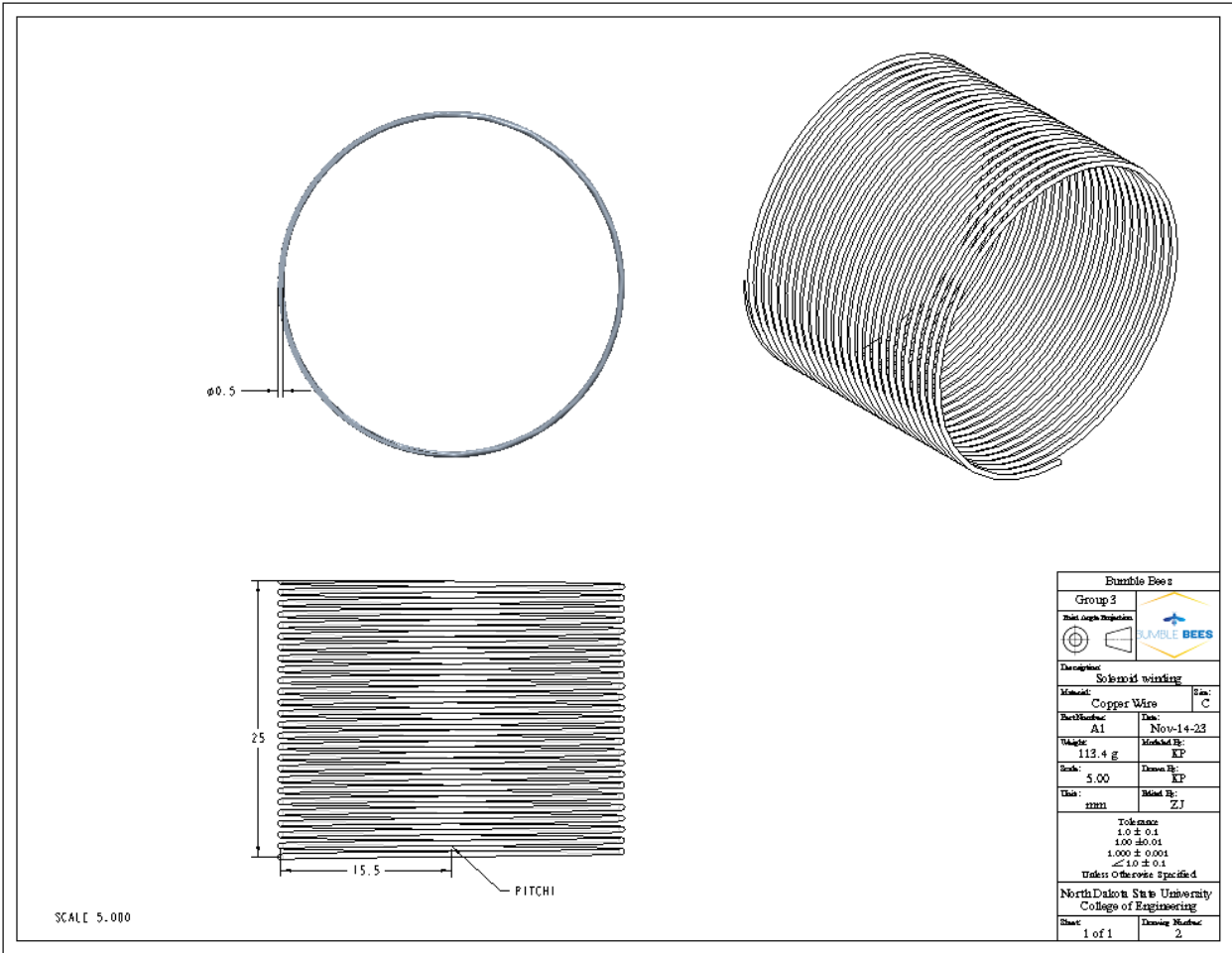
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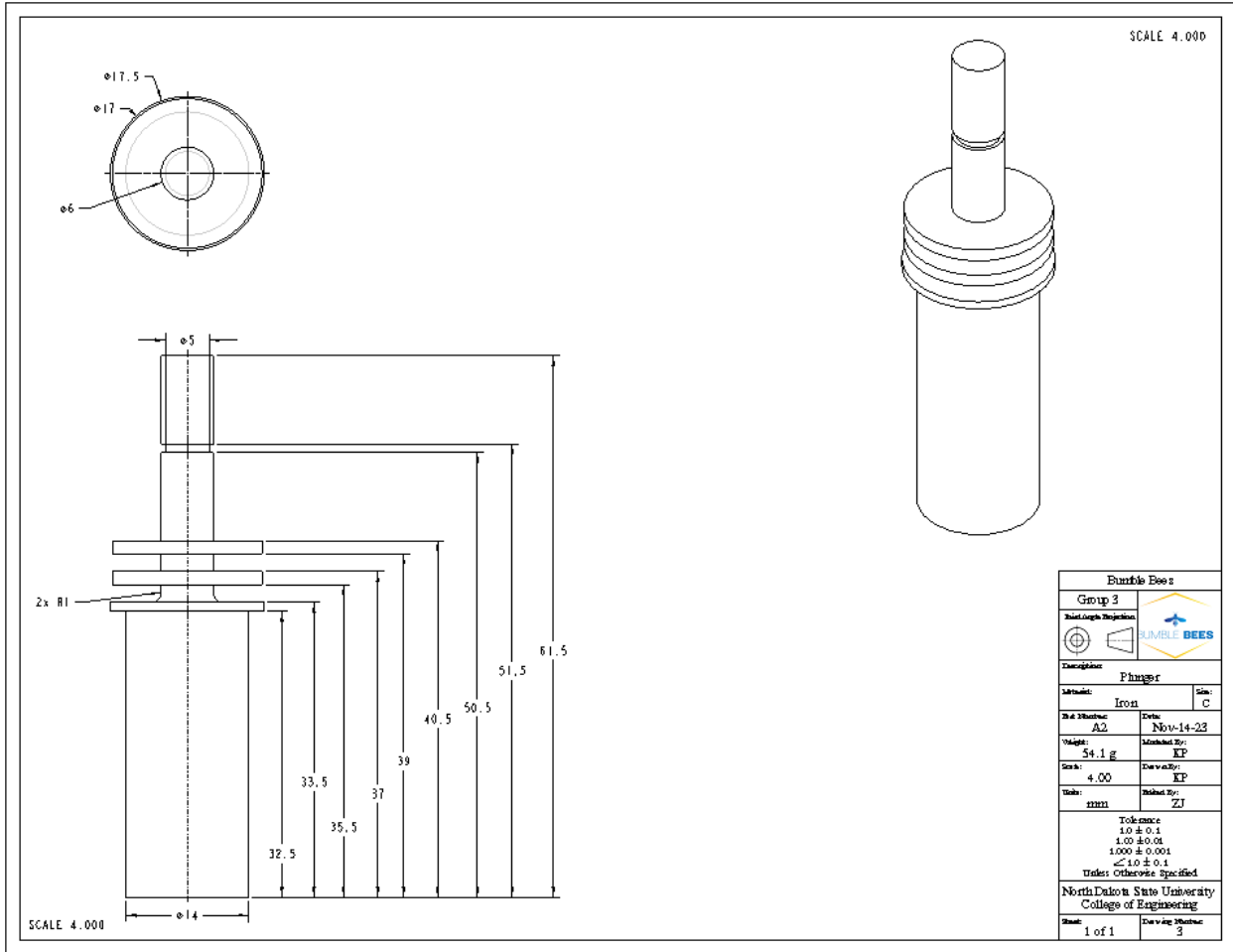


[A] SOLENOID SUBASSEMBLY

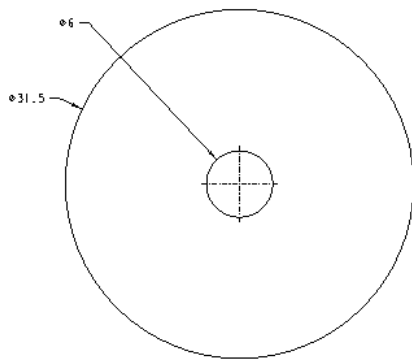
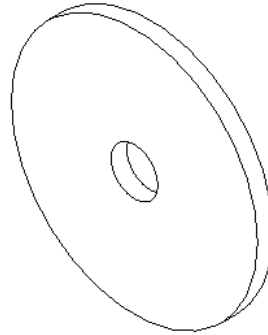


[A] ASSEMBLY DRAWINGS



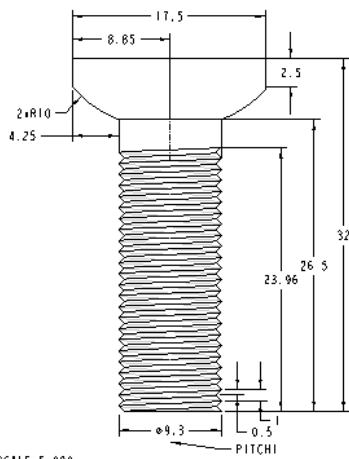
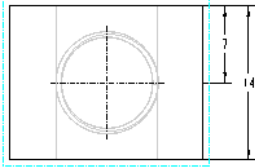


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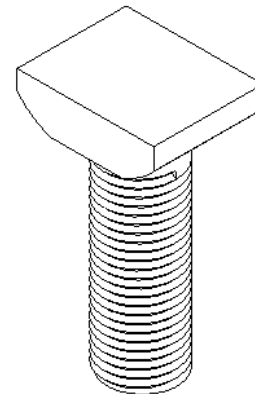


SCALE 5.000


Bumble Bee z	
Group 3	
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Material: Copper	Part: C
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Weight: 8.3 g	Manufact By: KP
Scale: 5.00	Drawn By: KP
Title: <u>zzzz</u>	Revised By: ZJ
Tolerances: 1.0 ± 0.1 1.00 ± 0.01 1.000 ± 0.001 ≤ 1.0 ± 0.1 Unless Otherwise Specified	
North Dakota State University College of Engineering	
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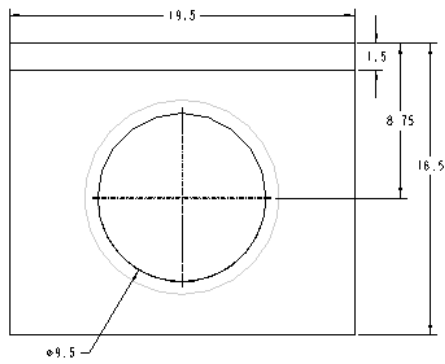
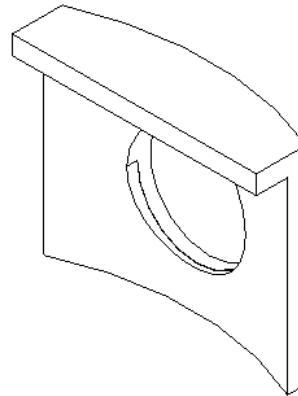
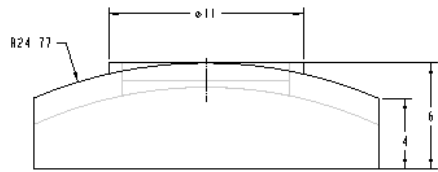
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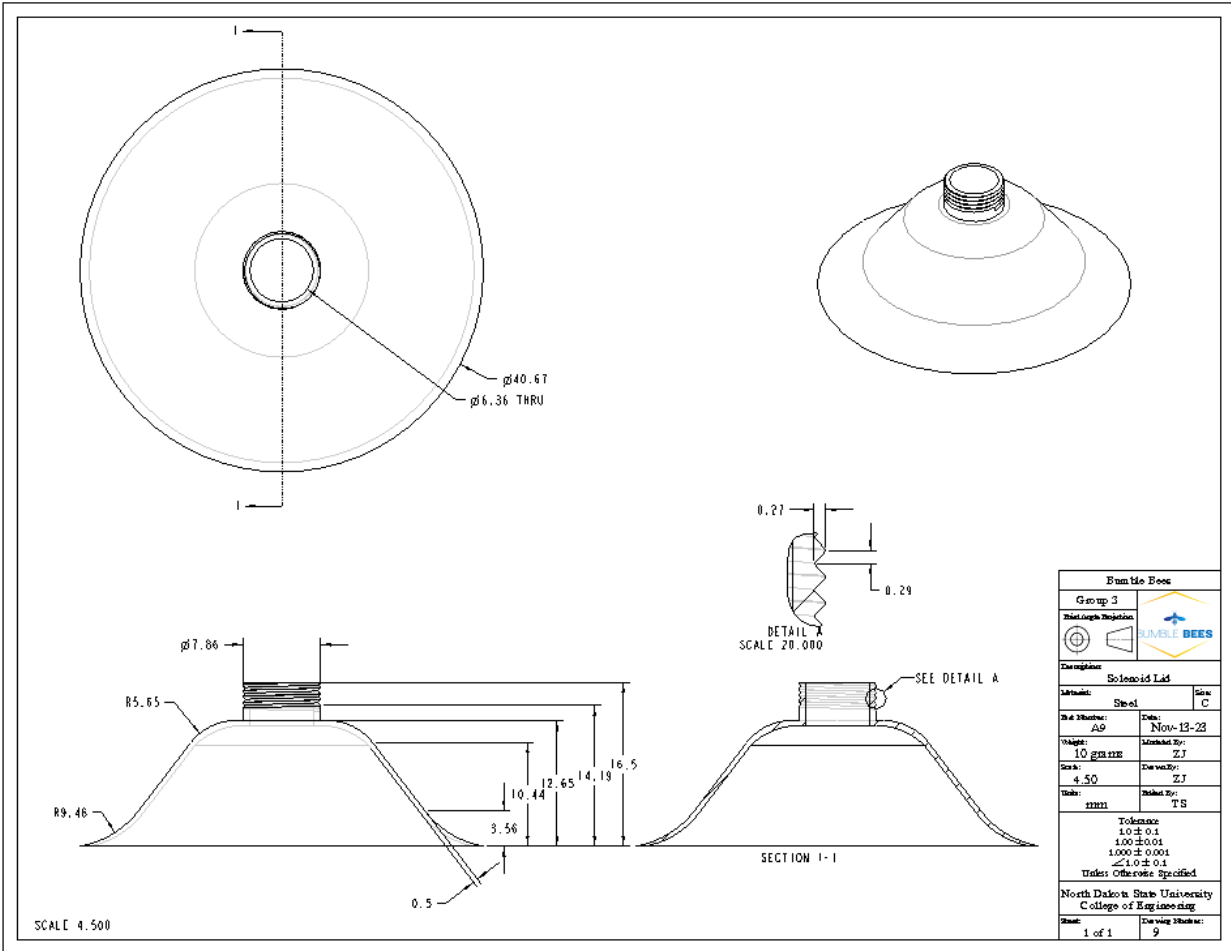
Bundle Boos	
Group 3	
Third Angle Projection	
Drawn by:	AMBL BEES
Description:	Field Bolt
Material:	Copper
Part Number:	AS
Order:	NOV-14-23
Weight:	23.8 g
Material Sp:	KP
Scale:	5.00
Drawn By:	KP
Title:	2221
Checked By:	ZJ
Tolerance 1.0 ± 0.1 1.00 ± 0.01 1.000 ± 0.001 ≤ 1.0 ± 0.1 Unless Otherwise Specified	
North Dakota State University College of Engineering	
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Drawing Number:	6


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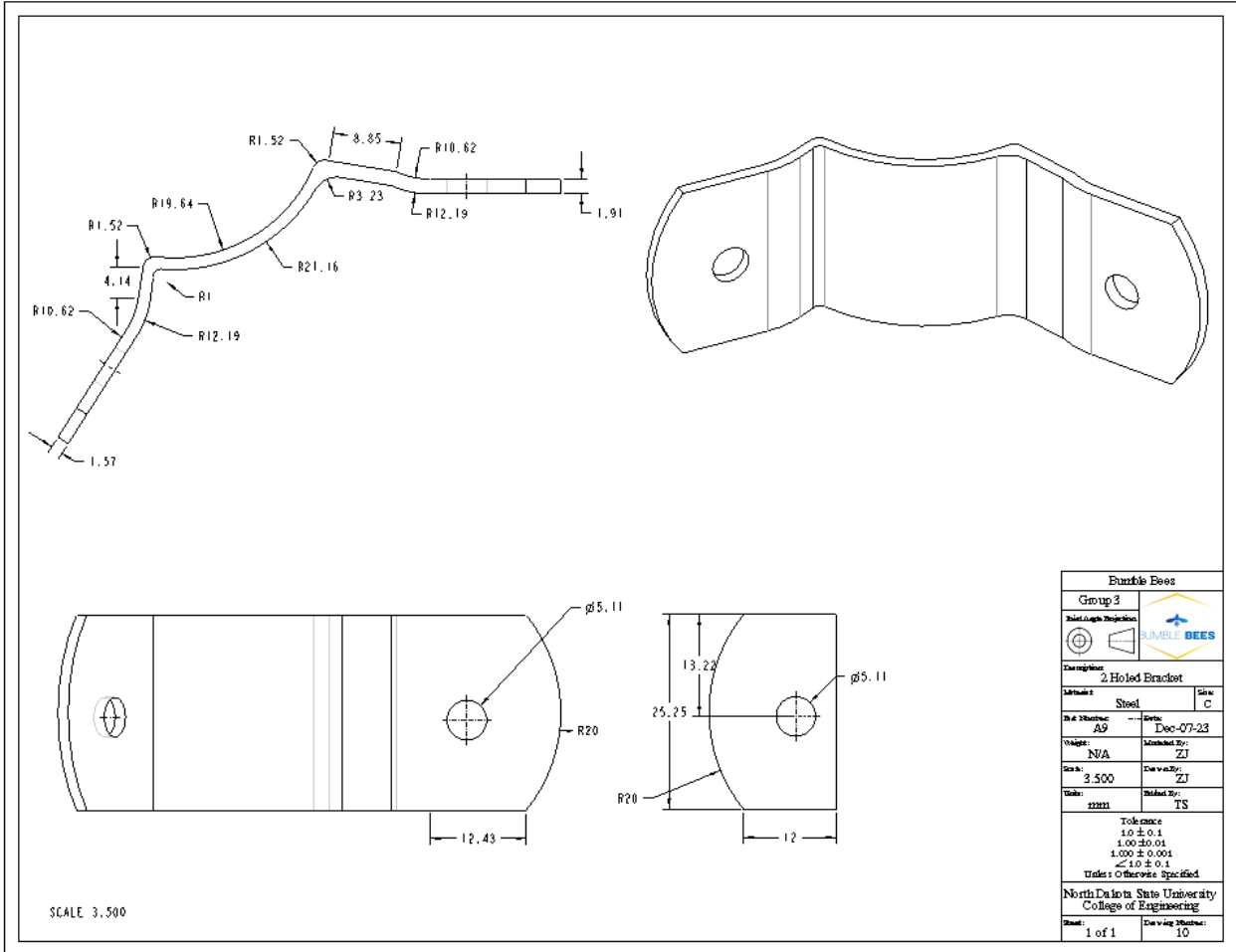


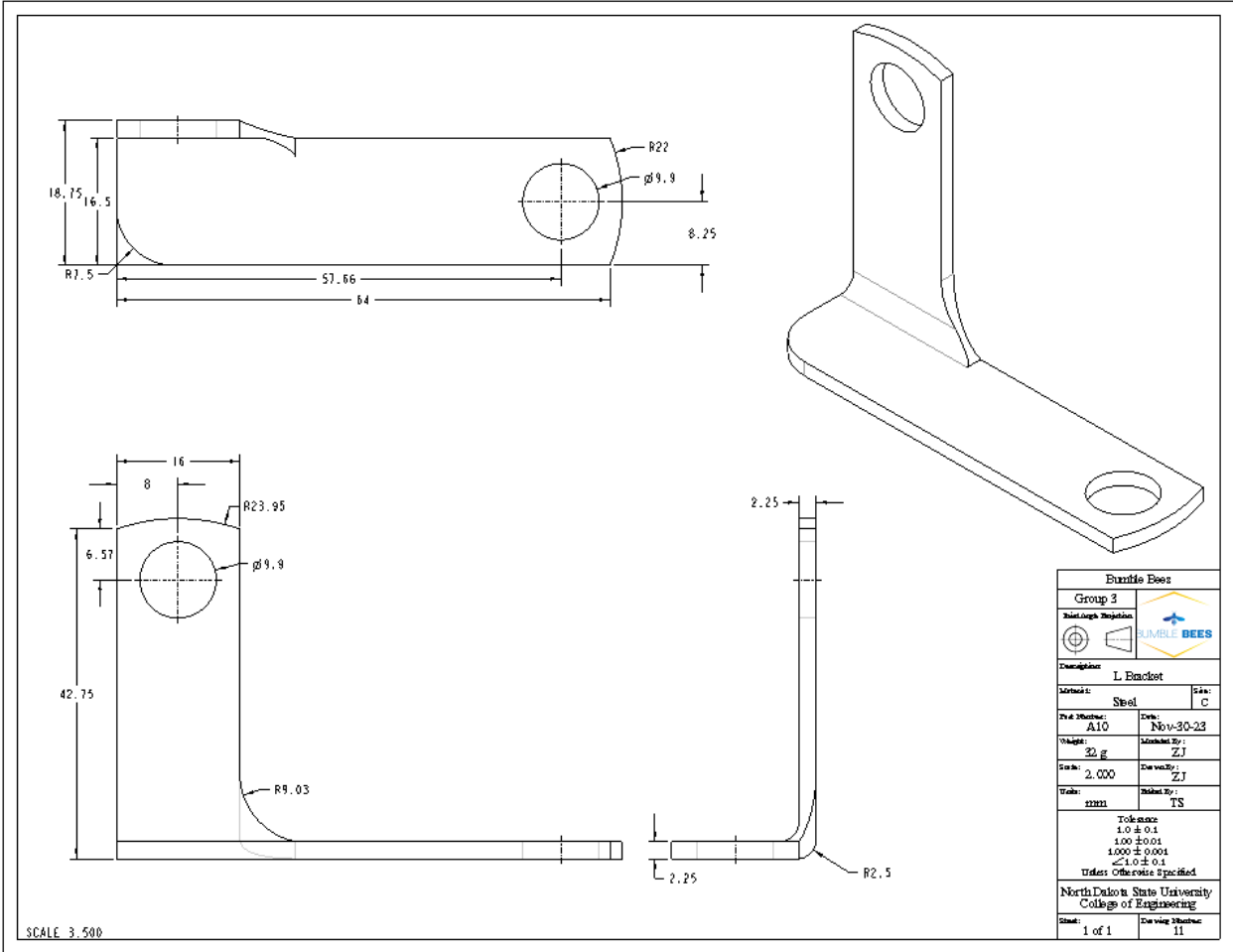
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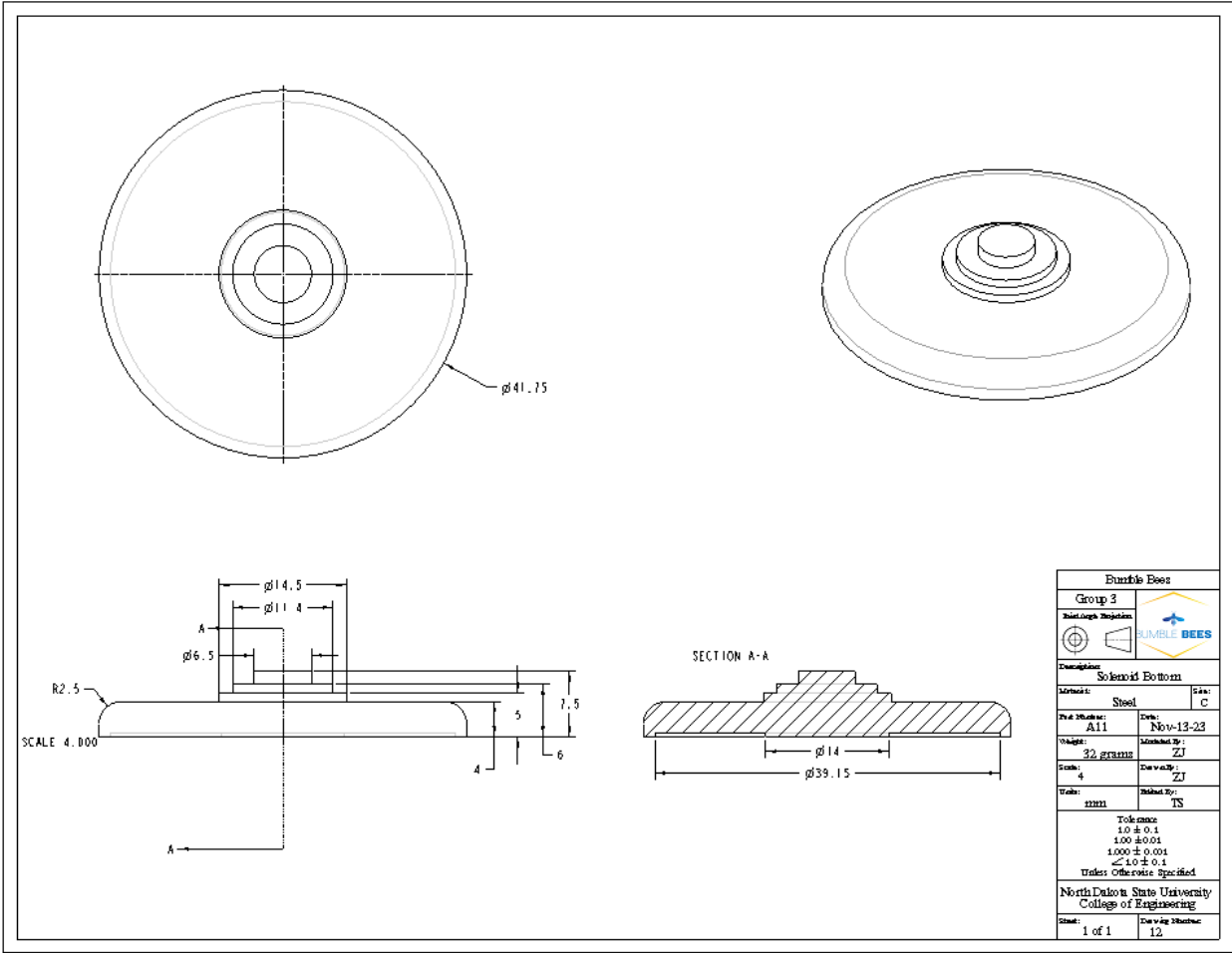
Rumble Bees	
Group 3	
	
Description: Rubber Stopper	
Material: Rubber	Size: C
Part Number: 26	Date: Nov-14-23
Weight: 0.7 g	Maker: KP
Size: 8.00	Die used: KP
File: 2221	Sheet No: 2/1
Tolerance 1.0 ± 0.1 1.00 ± 0.01 1.000 ± 0.001 < 1.0 ± 0.1 Unless Otherwise Specified	
North Dakota State University College of Engineering	
Sheet: 1 of 1	Drawing Number: 7



Solenoid Lid	
Group 3	
North Dakota State University	
Drawn by: [Symbol]	Checked by: [Symbol]
Material: Steel	Scale: C
Date: Nov-12-23	
Weight: 10 gm	Lot: ZJ
Size: 4.50	Drawn by: ZJ
Unit: mm	Checked by: TS
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North Dakota State University College of Engineering	
Sheet: 1 of 1	Revision Number: 9





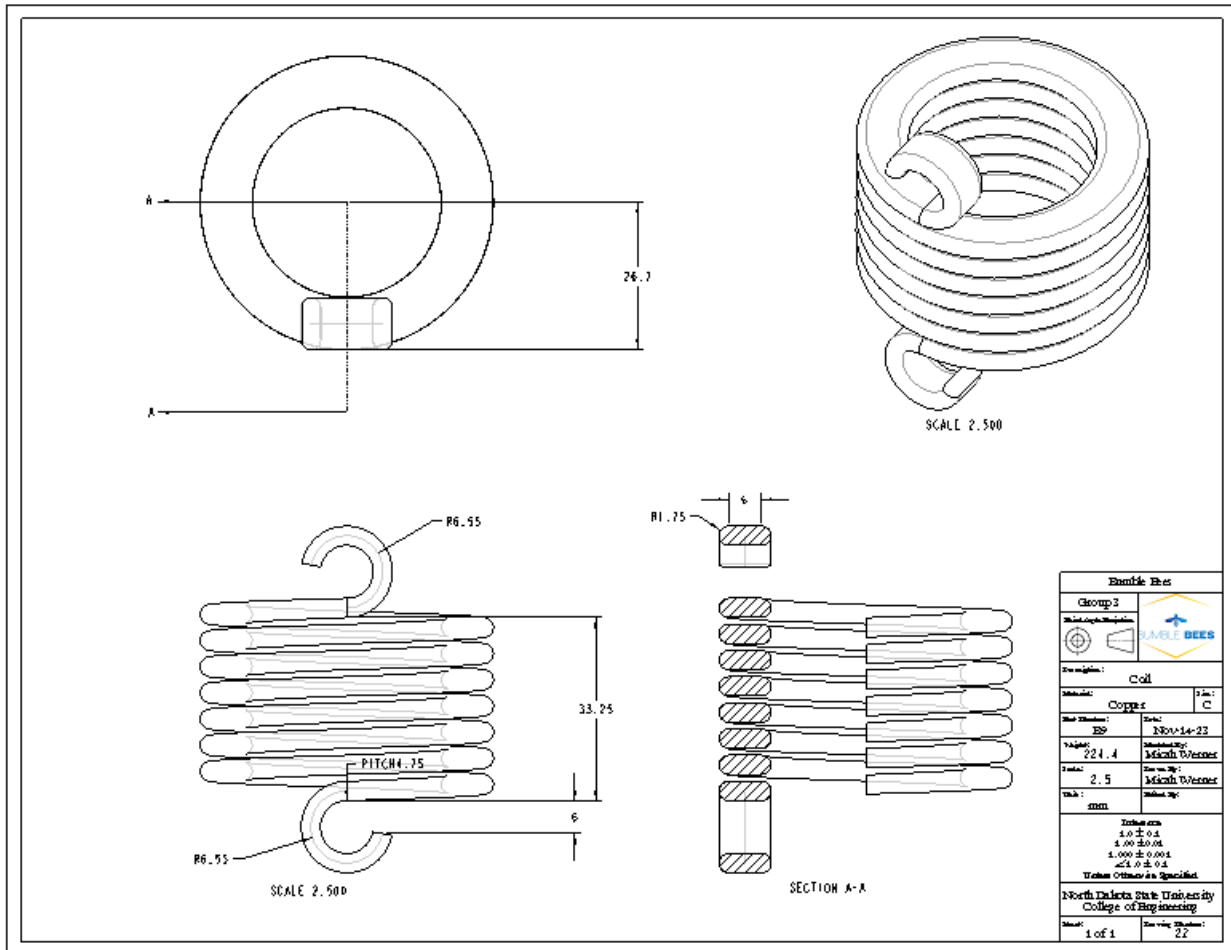


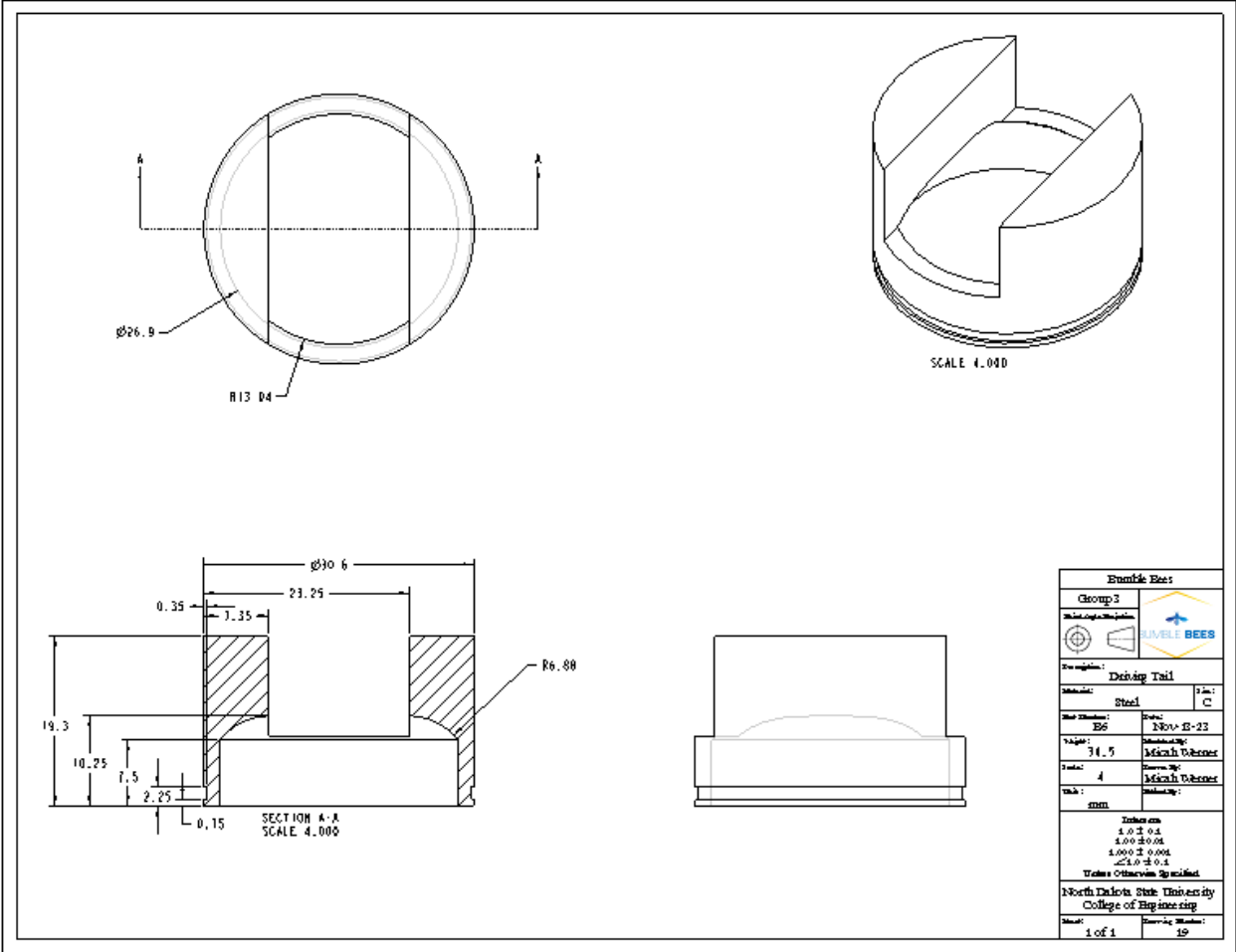
[B] DRIVE SUBASSEMBLY

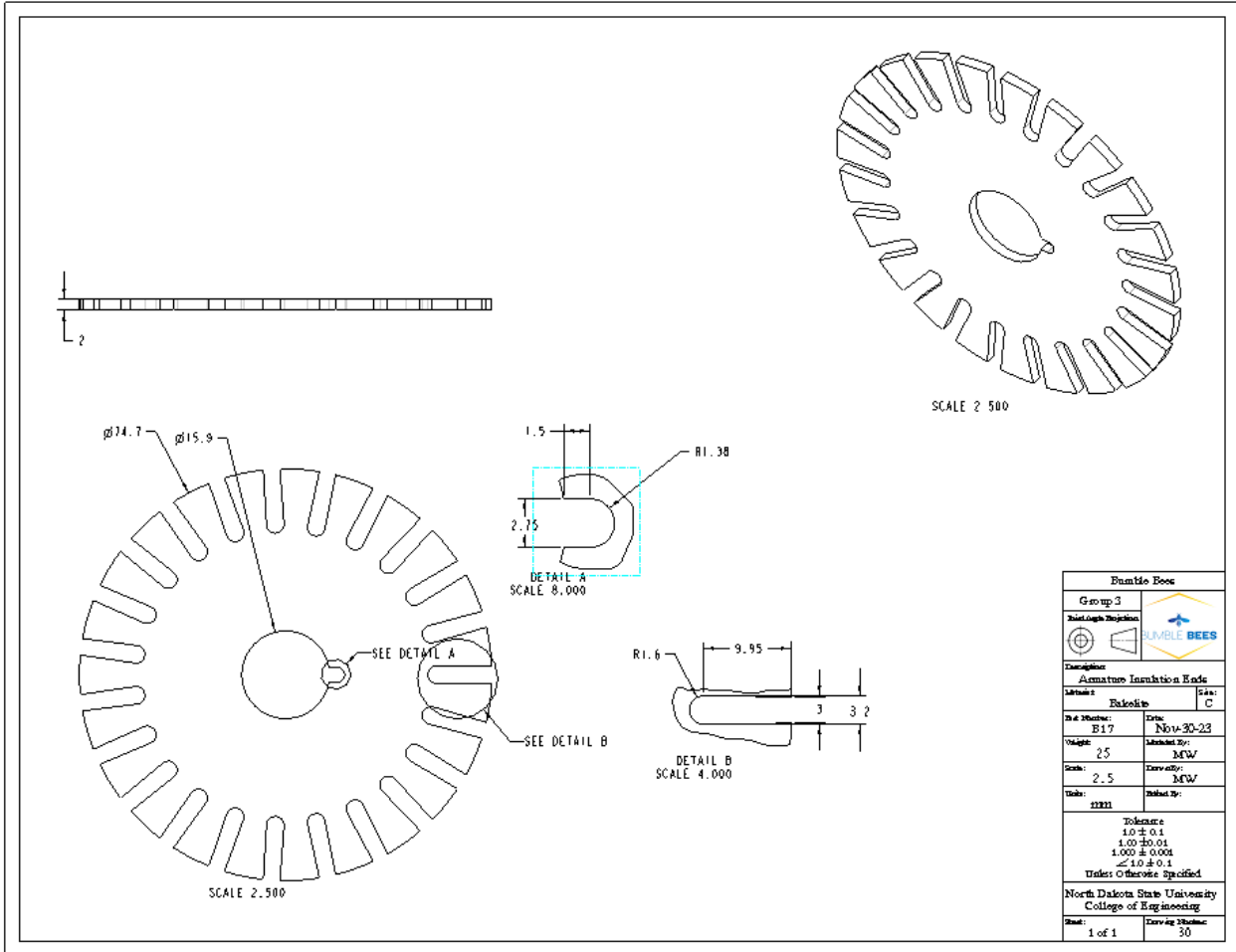
Drive Sub Assembly			
Part #	Part Name	Quantity	Material
SP22	Washer	1	Steel
E2	Shaft	1	Steel
E3	Commutator	1	Copper
E4	Armature Insulation Sheet Bottom	2	Epoxyite
E5	Sleeve Washer	1	Steel
E6	Driving Tail	1	Steel
E7	Driving Head	1	Steel
E8	Multifurcated Sleeve	1	Steel
E9	Coil	1	Copper
B10	Hexid Screw	2	Steel
B11	Pinion	1	Steel
B12	Armature P&S	58	Steel
B13	Pinion Stop	1	Steel
B14	Armature Winda Top	1	Steel
B15	Armature Insulation Shell	23	Epoxyite
B16	Armature Winda Bottom	1	Steel
B17	Armature Insulation Ends	2	Epoxyite
B18	Armature Insulation Sheet Top	1	Epoxyite
B19	Inside Commutator 1	1	Steel
E20	Inside Commutator 2	1	Steel

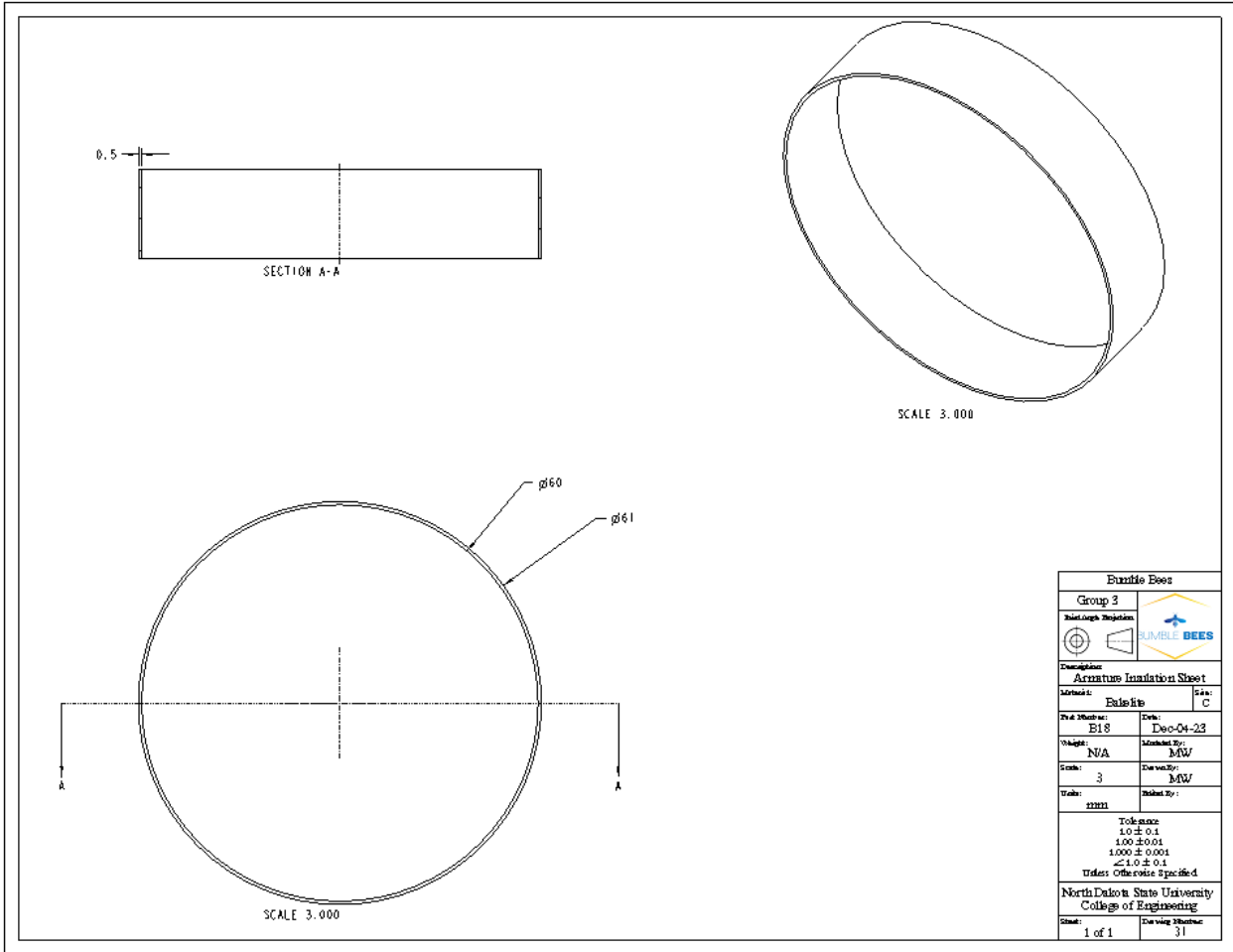
Bumble Bees			
Group 3			
Description: Armature Assembly			
Material:	various	Size:	C
Part Number:	B	Date:	Dec-05-23
Weight:	22lb	Designed By:	MW, TASN
Scale:	0.5	Drawn By:	MW
Title:	22221	Checked By:	TASN
Tolerance: 1.0 ± 0.1 1.00 ± 0.01 1.000 ± 0.001 < 1.0 ± 0.1 Unless Otherwise Specified			
North Dakota State University College of Engineering			
Sheet:	1 of 1	Drawing Number:	13

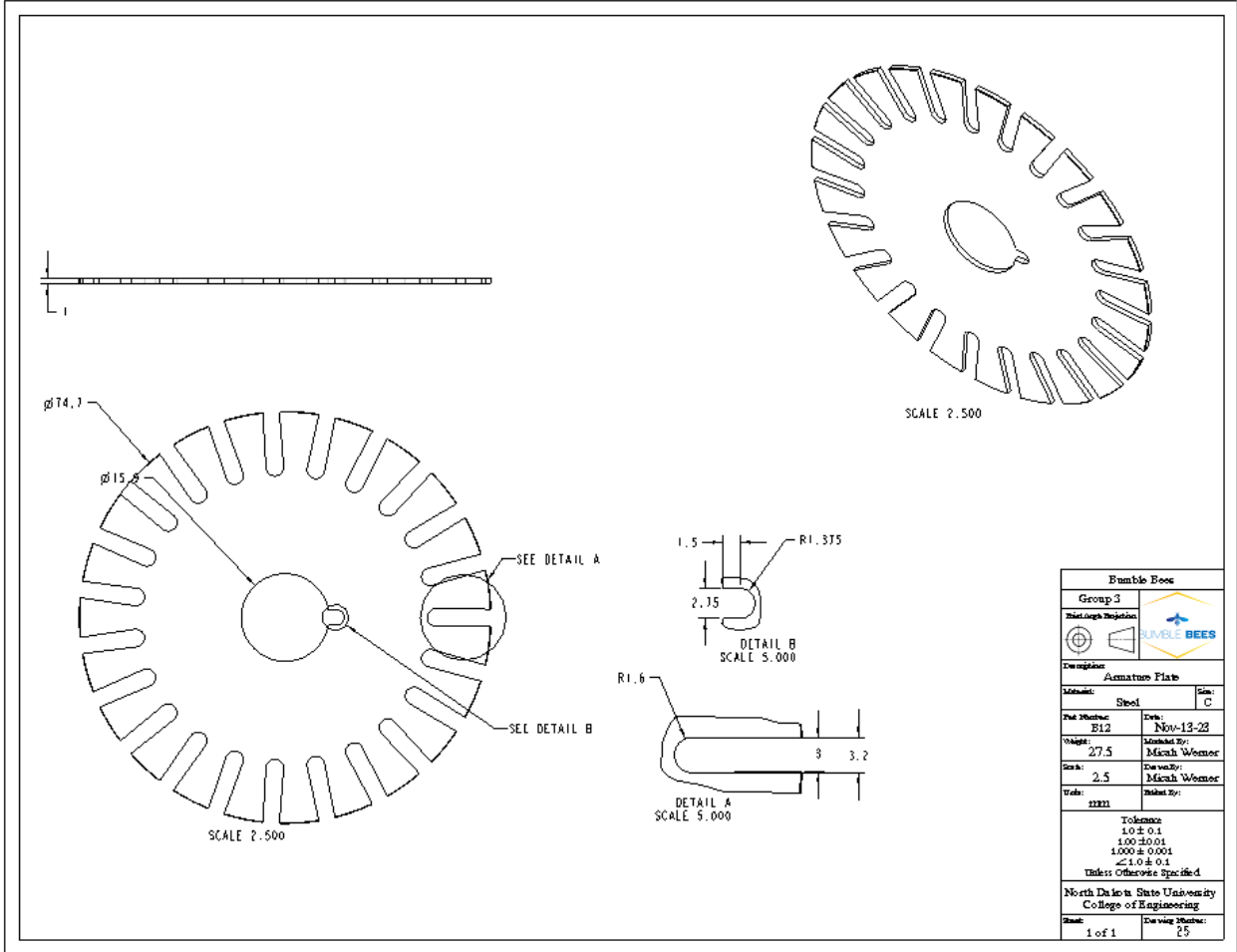
[B] ASSEMBLY DRAWINGS

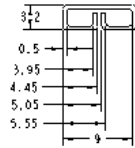




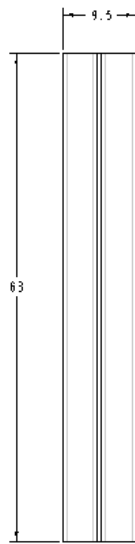










*All rounds are R0.5

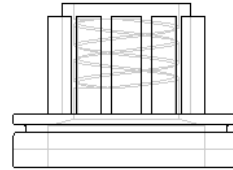
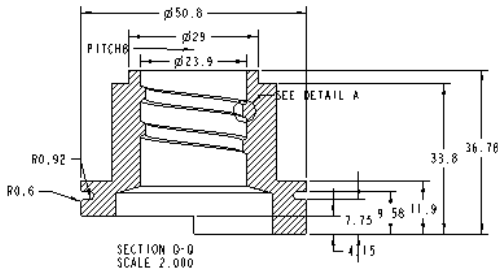
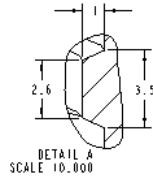
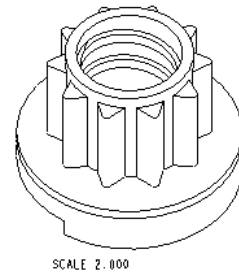
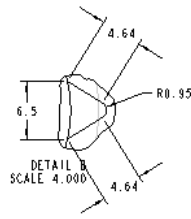
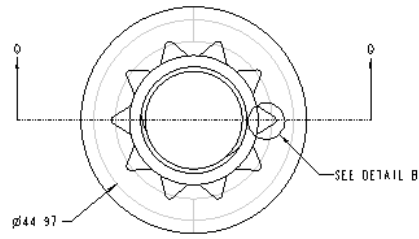




SCALE 3.500

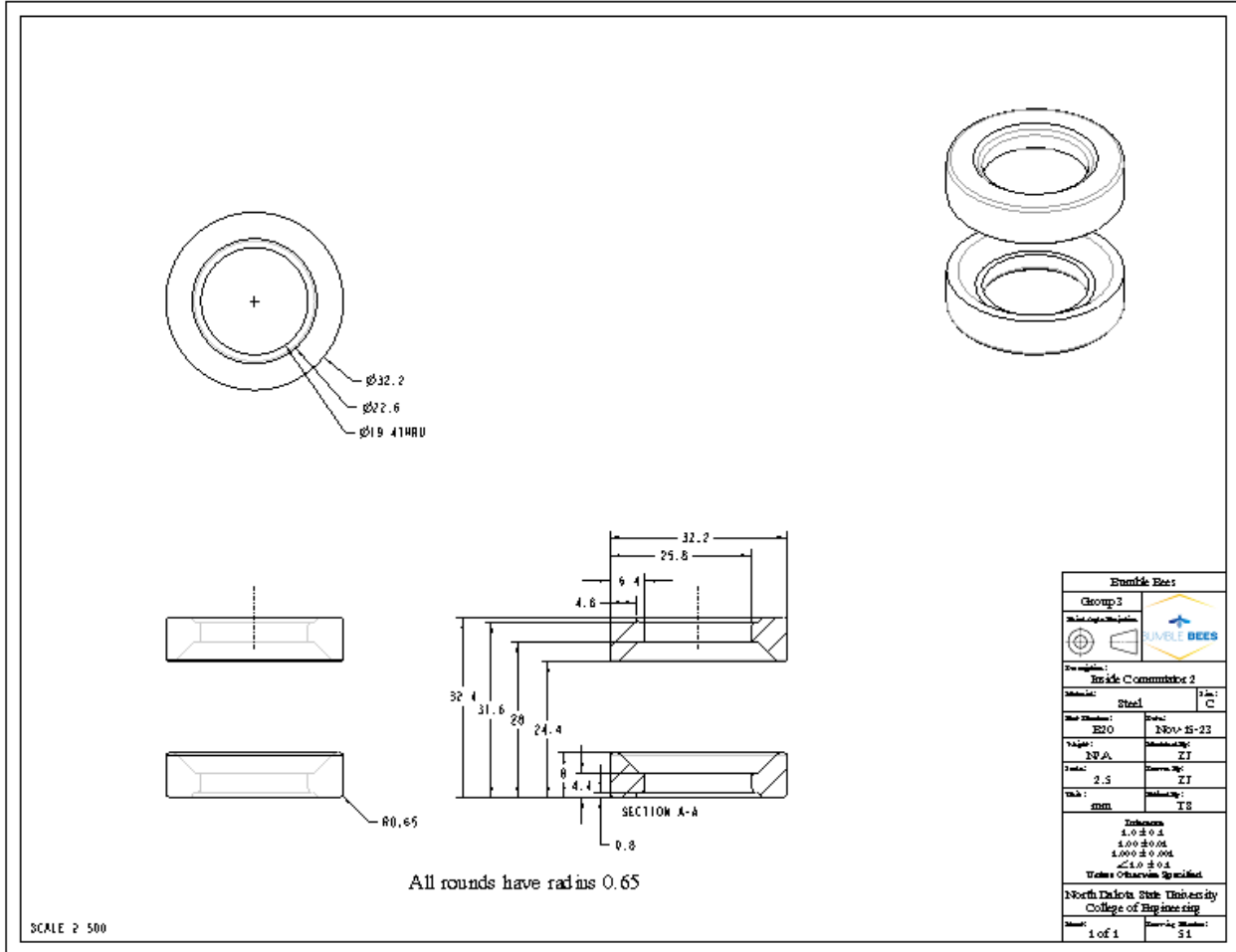


SCALE 3.500

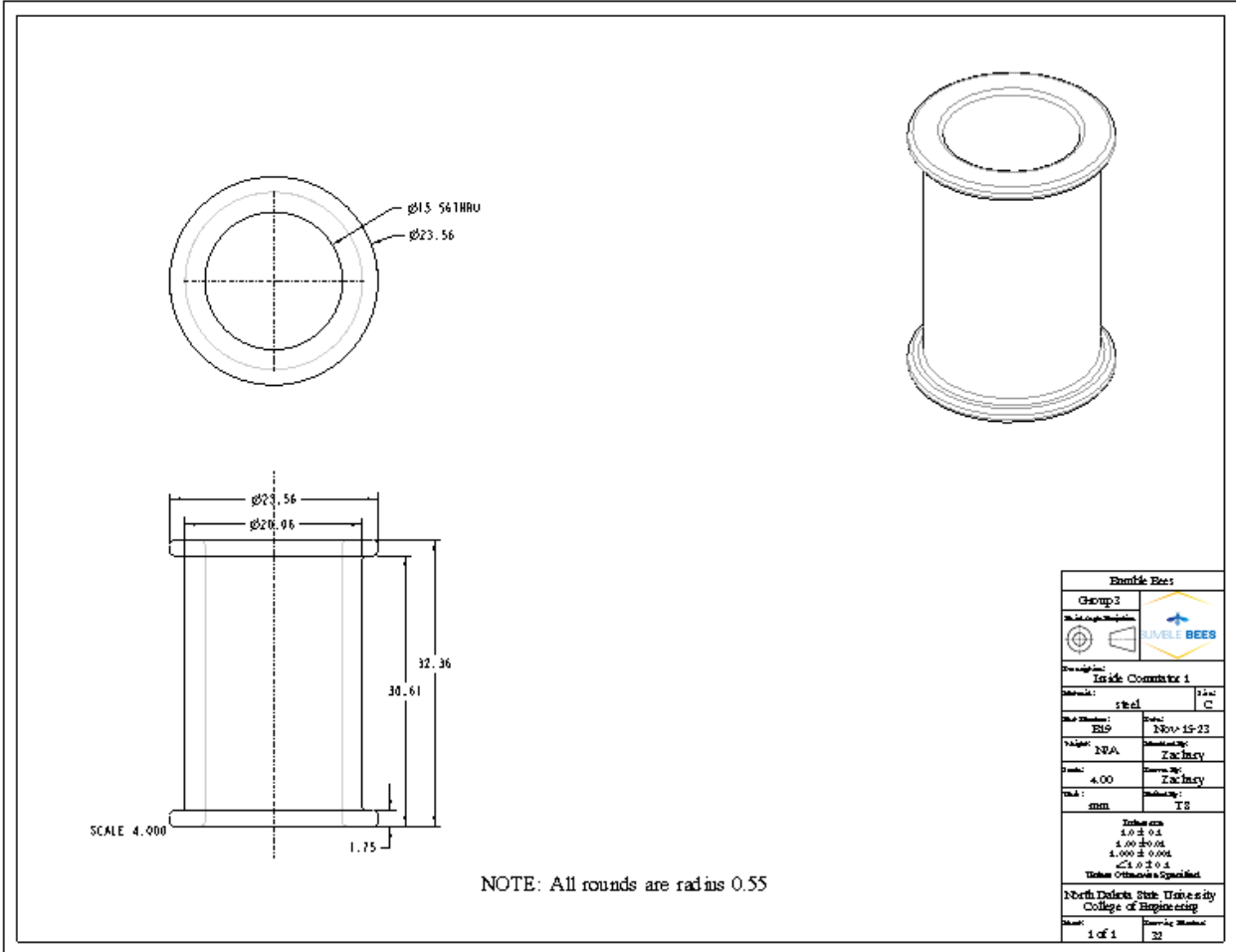
Bumble Bee	
Group 3	
 	
Description: Insulation Shell	
Address: <u>Ridgely</u>	Size: <u>C</u>
Date: <u>Nov-30-23</u>	Date: <u>Nov-30-23</u>
Design: <u>EW</u>	Checked By: <u>MW</u>
Scale: <u>3.5</u>	Drawn By: <u>MW</u>
Title: <u>2221</u>	Made By:
Tolerances: 1.0 ± 0.1 1.00 ± 0.01 1.000 ± 0.001 < 1.0 ± 0.1 Unless Otherwise Specified	
North Dakota State University College of Engineering	
Sheet: <u>1 of 1</u>	Drawing Number: <u>28</u>




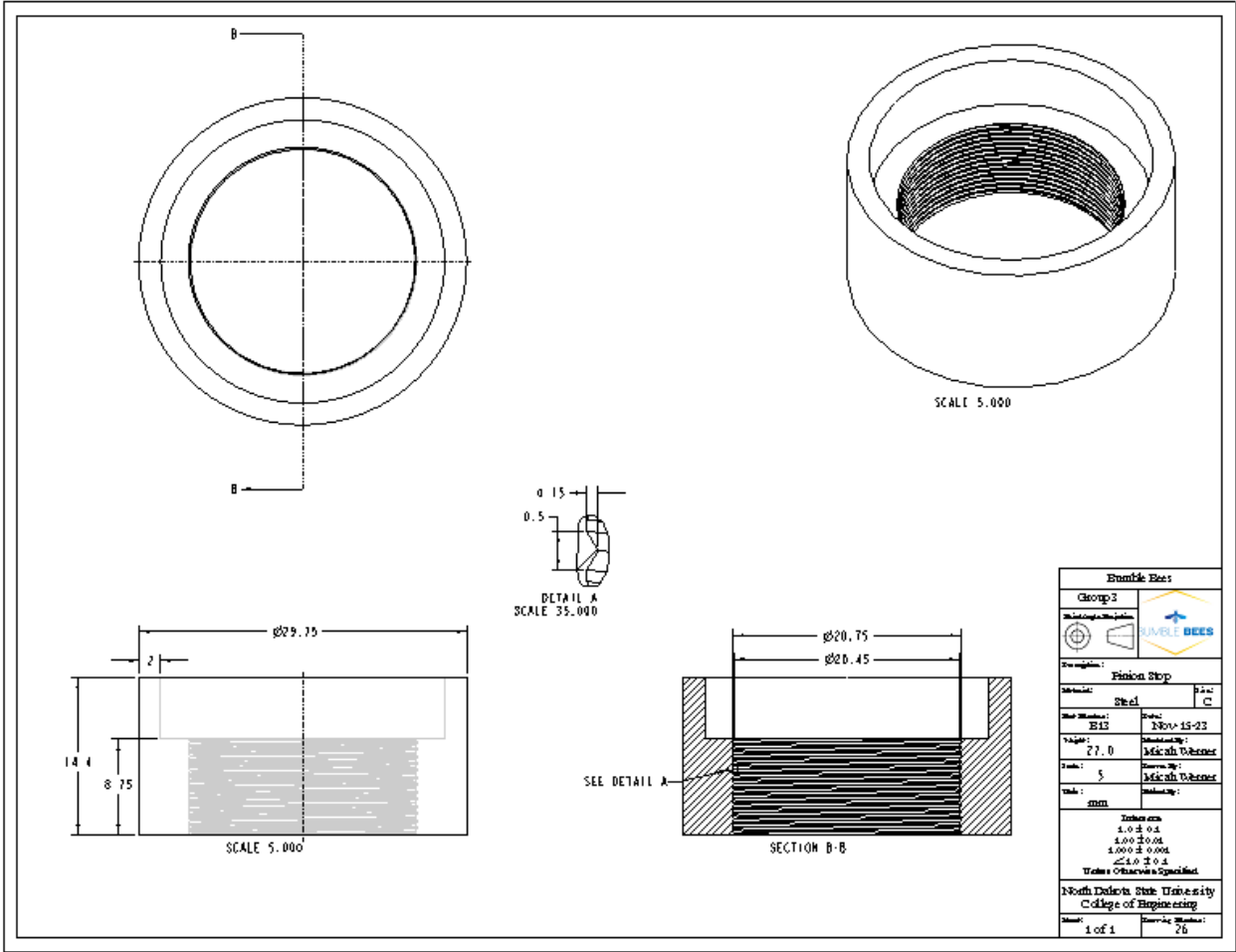
Bumble Bees	
Group 3	
	
Assignment: Pinion	
Material: Steel	Case: C
Std. Number: B11	Date: Nov-13-23
Weight: 167.0	Submitted By: Manli Werner
Size: 2	Drawn By: Manli Werner
Title: #22021	Checked By:
Tolerances 1.00 ± 0.1 1.00-20.01 1.000 ± 0.001 <math>< 1.00 \pm 0.1</math> Unless Otherwise Specified	
North Carolina State University College of Engineering	
Sheet: 1 of 1	Engineering Number: 24

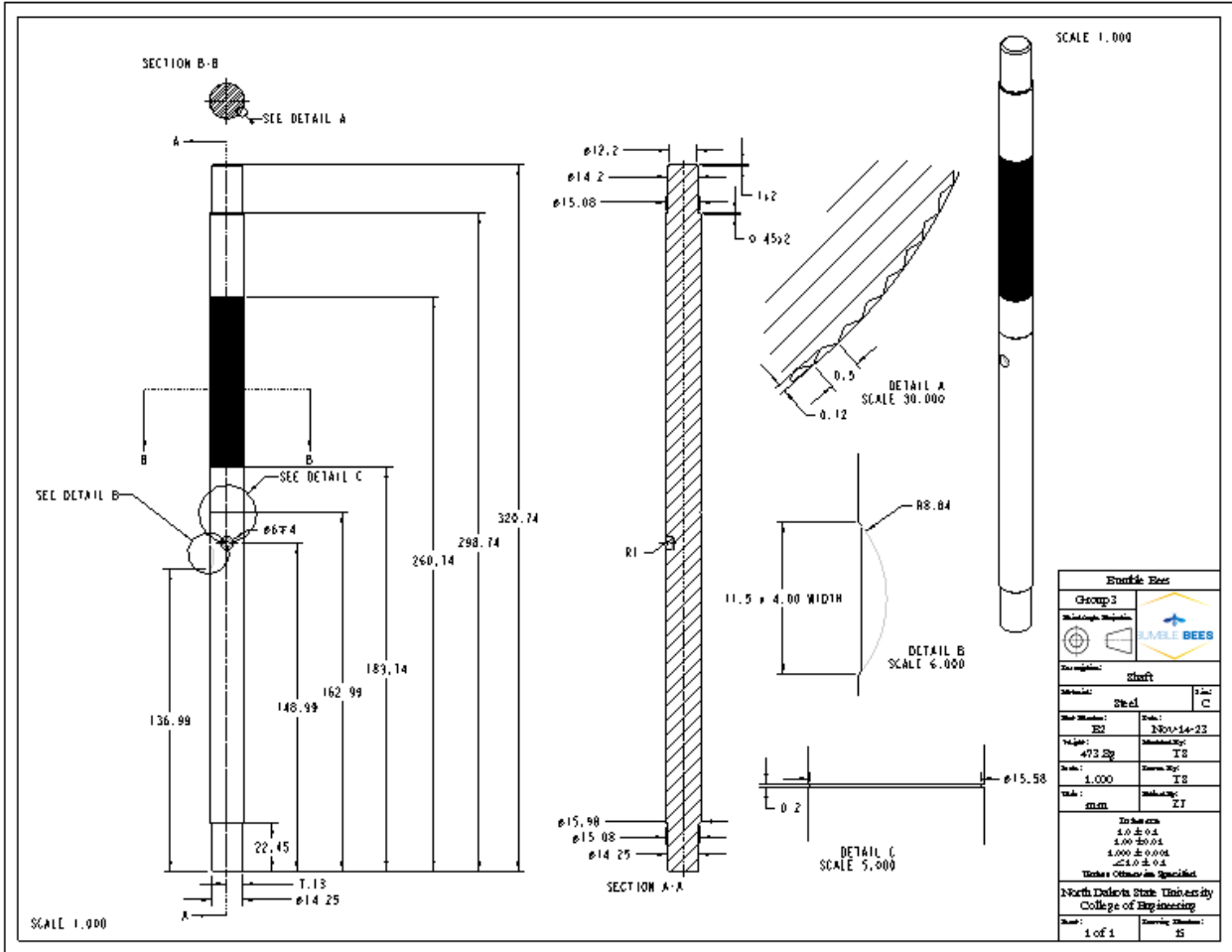


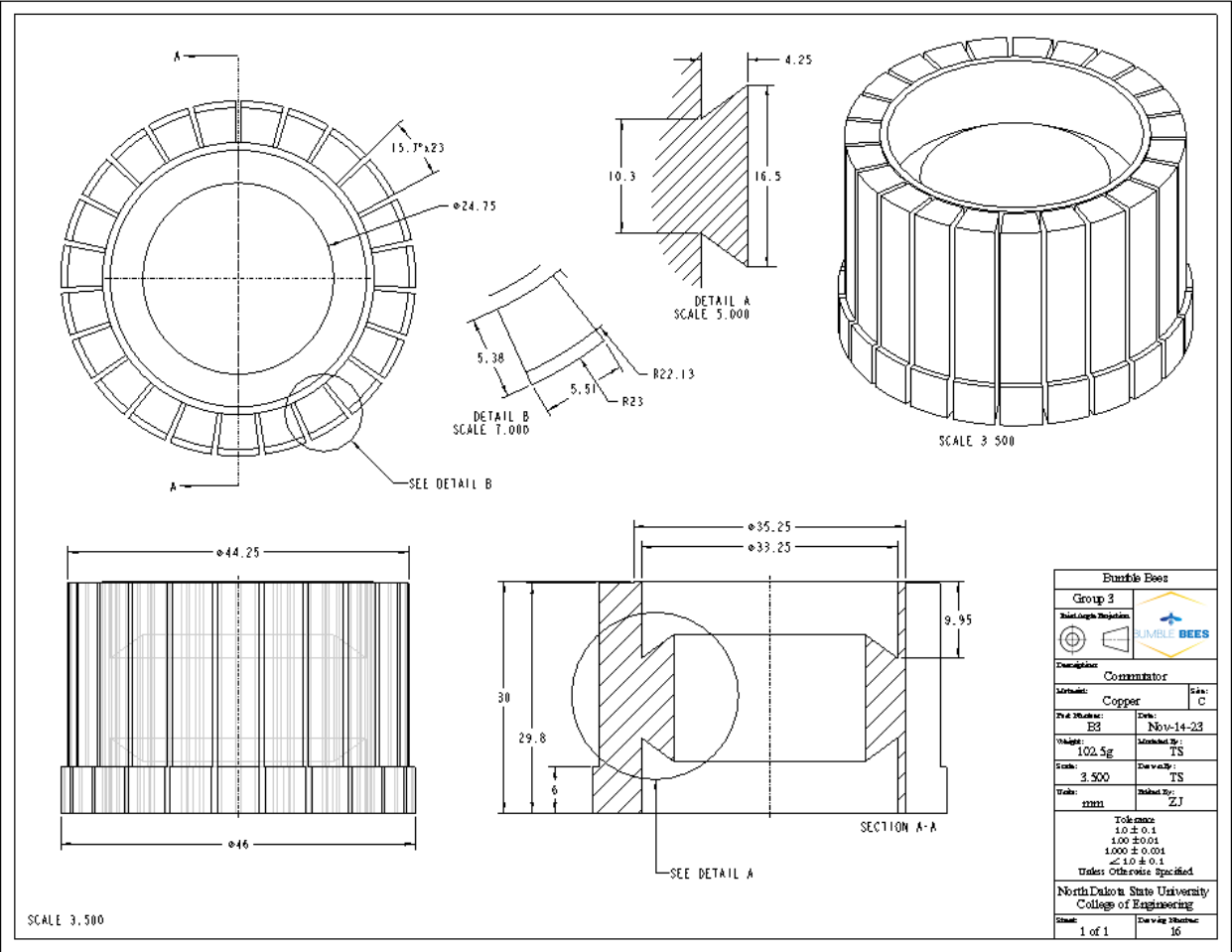
SCALE 2:500



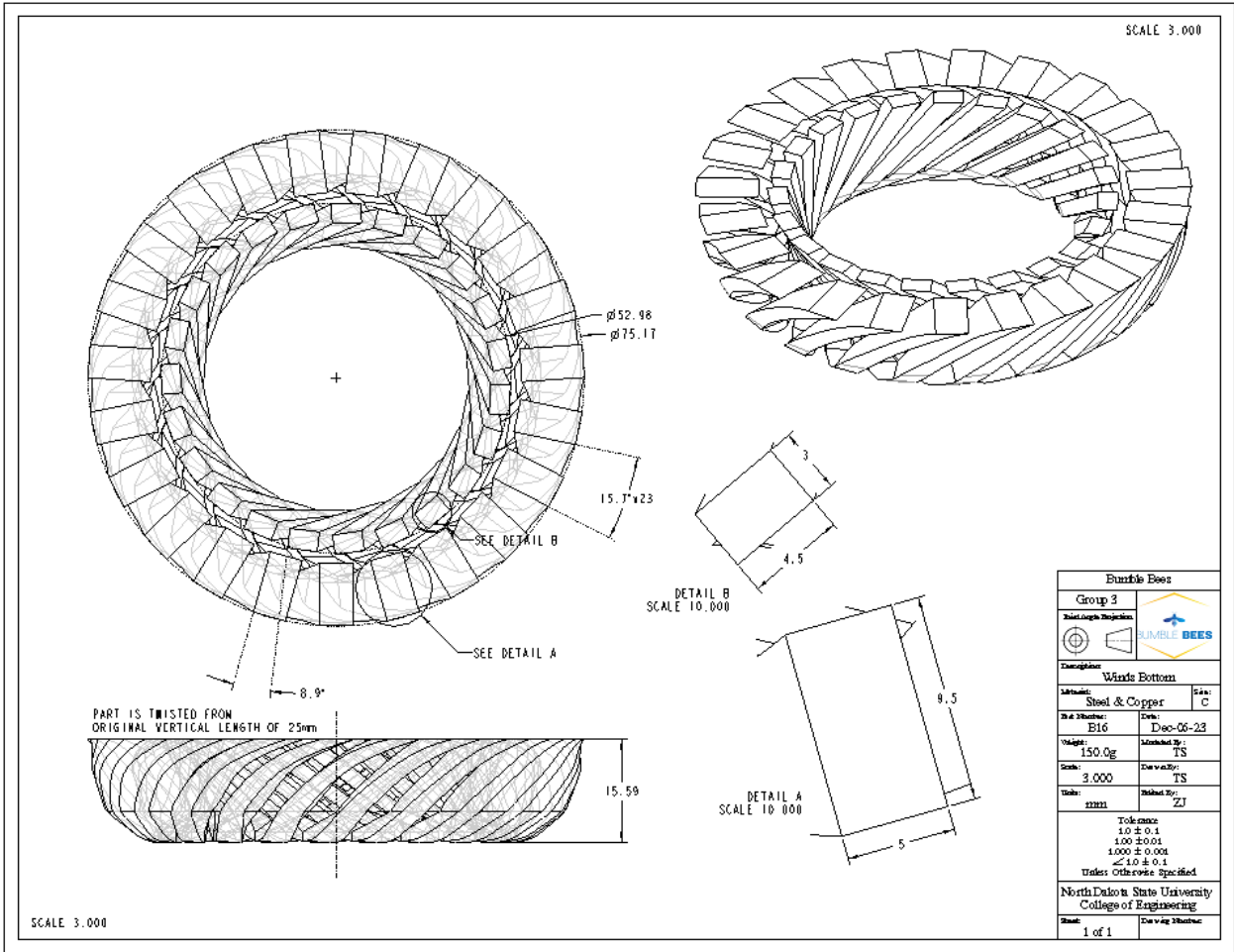
Bumble Bees	
Group 3	
	
Description: Inside Connector 1	
Material: steel	Part: C
Rev Number: B19	Date: Nov-15-23
Weight: N/A	Manufacturer: ZACHRY
Cost: 4.00	Source No: ZACHRY
Unit: mm	Industry: TS
Tolerances: 1.00 ± 0.4 1.00 ± 0.04 1.00 ± 0.004 0.25 ± 0.1 Unless Otherwise Specified	
North Dakota State University College of Engineering	
Sheet: 1 of 1	Drawing Number: 22

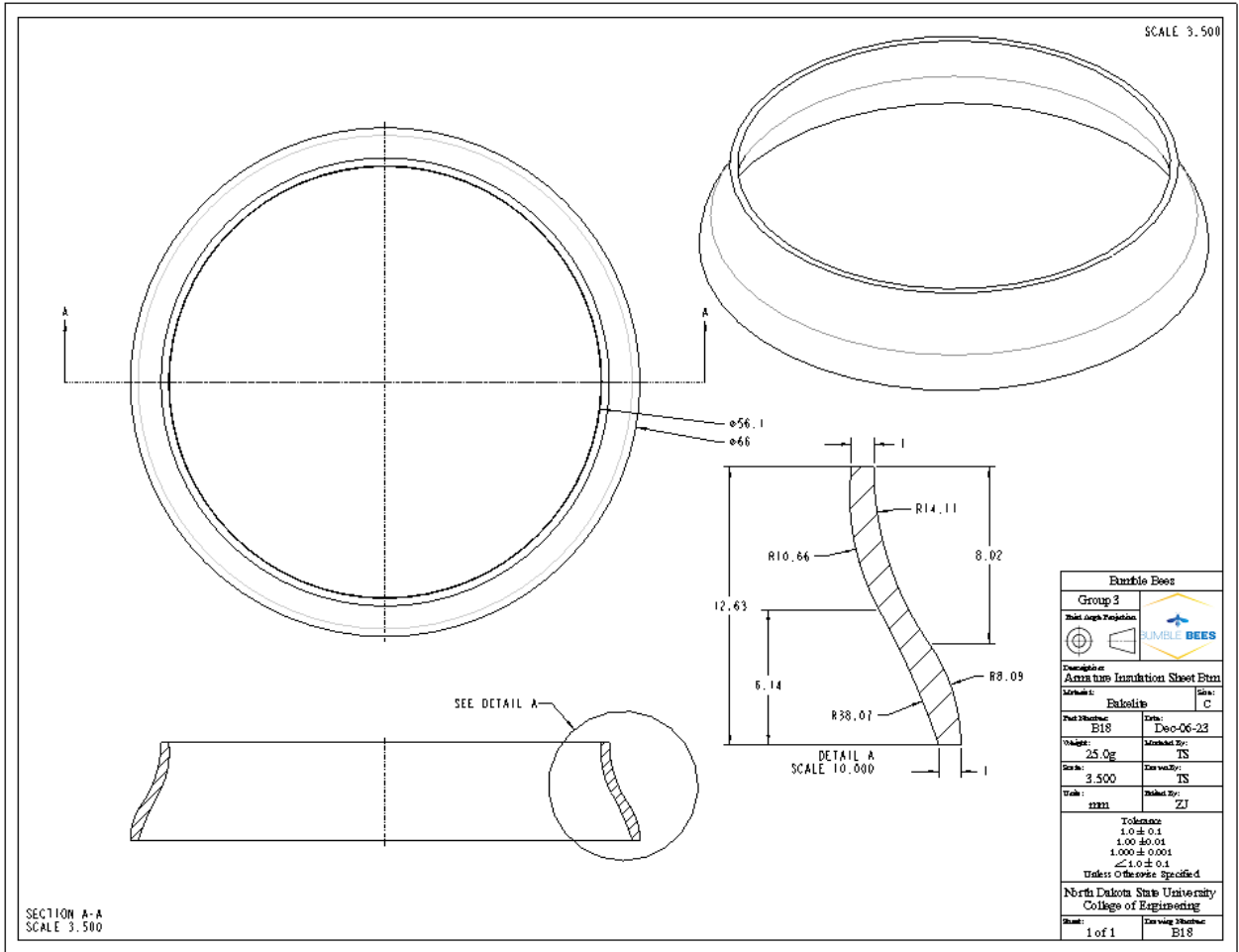








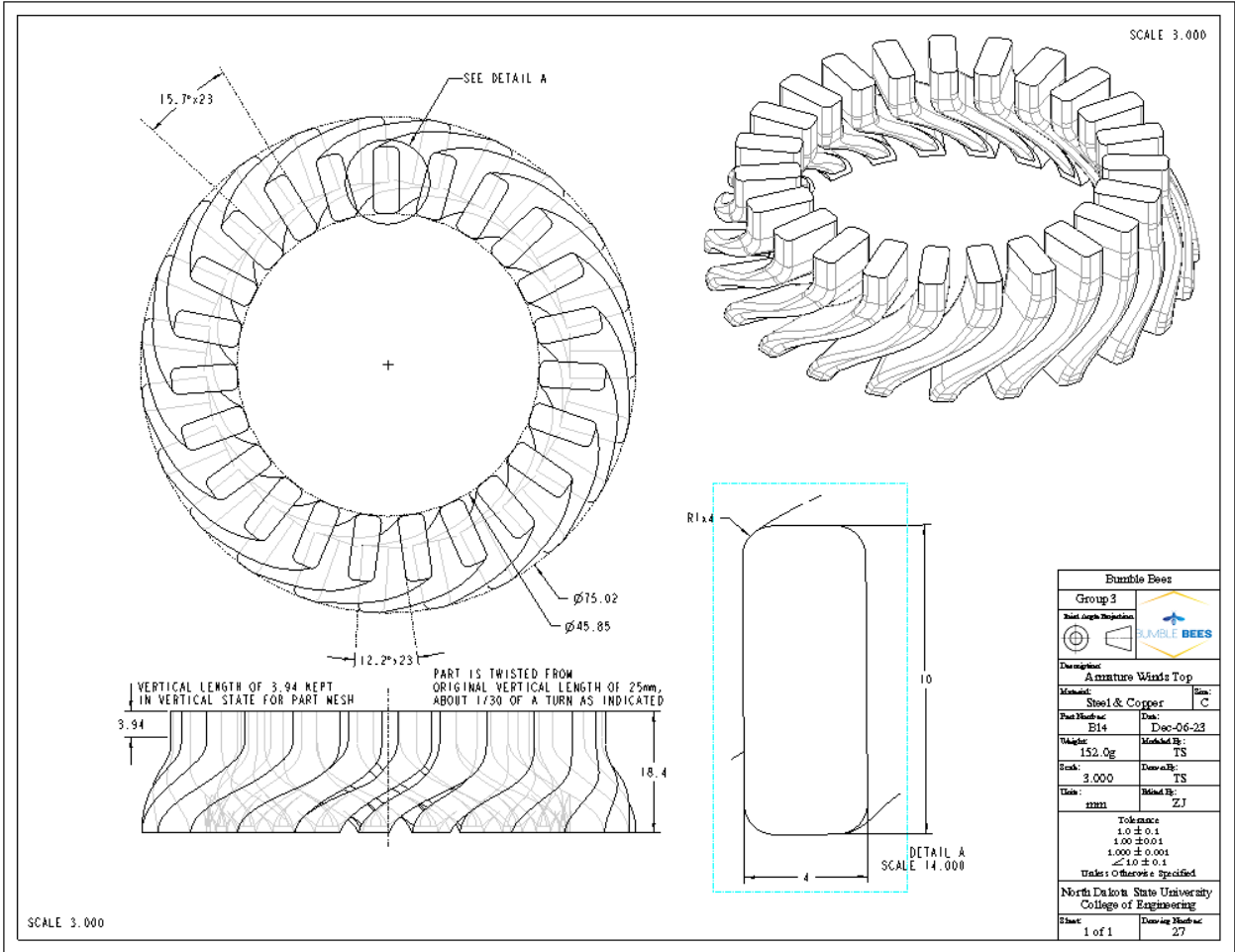
Bumble Bees	
Group 3	
Student Registration	
Description: Commutator	
Material: Copper	Size: C
Part Number: ES	Date: Nov-14-23
Weight: 102.5g	Insulated By: TS
Scale: 3.500	Drawn By: TS
Units: mm	Checked By: ZJ
Tolerances: 1.0 ± 0.1 1.00 ± 0.01 1.000 ± 0.001 $< 1.0 \pm 0.1$ Unless Otherwise Specified	
North Dakota State University College of Engineering	
Sheet: 1 of 1	Drawing Number: 16

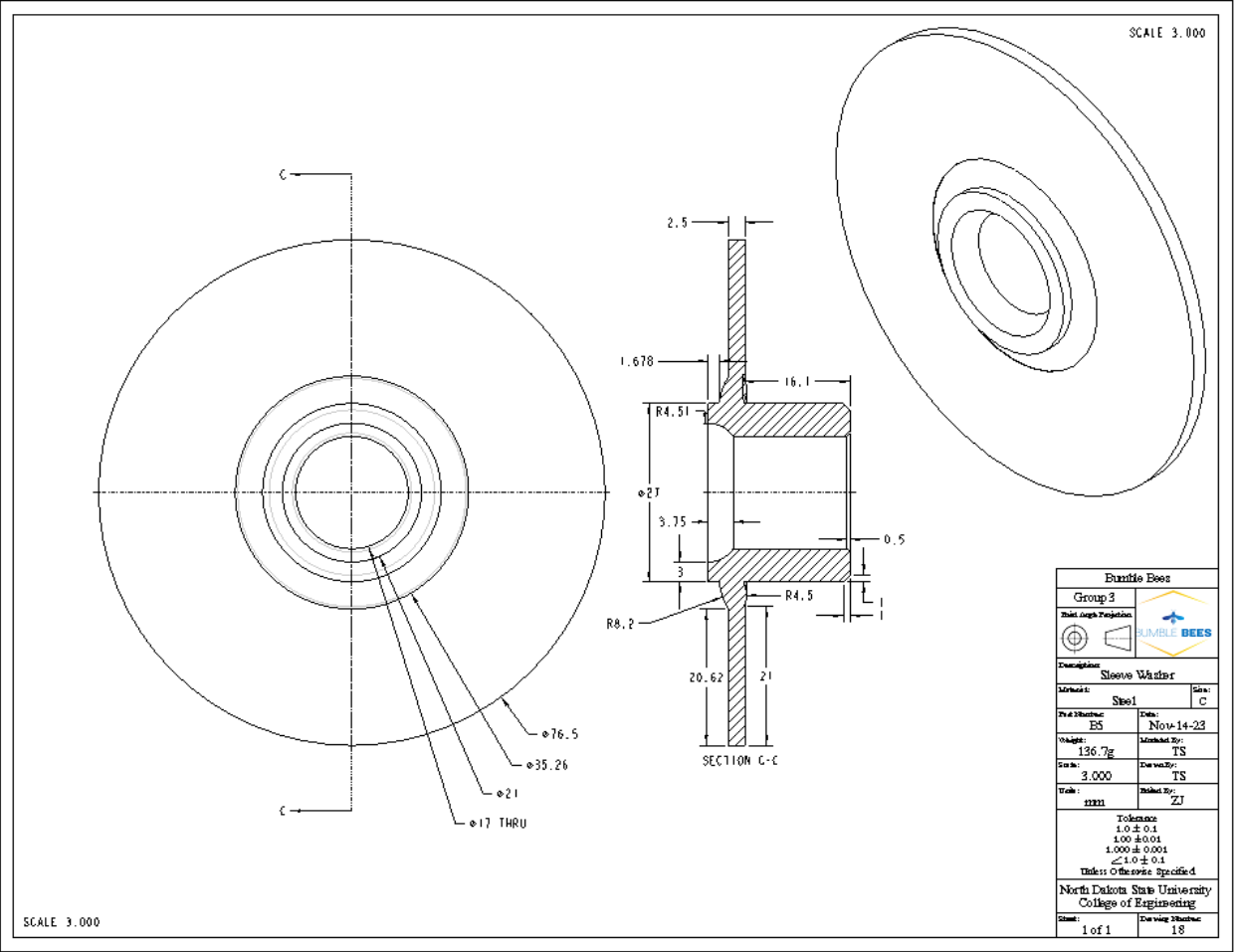


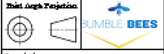



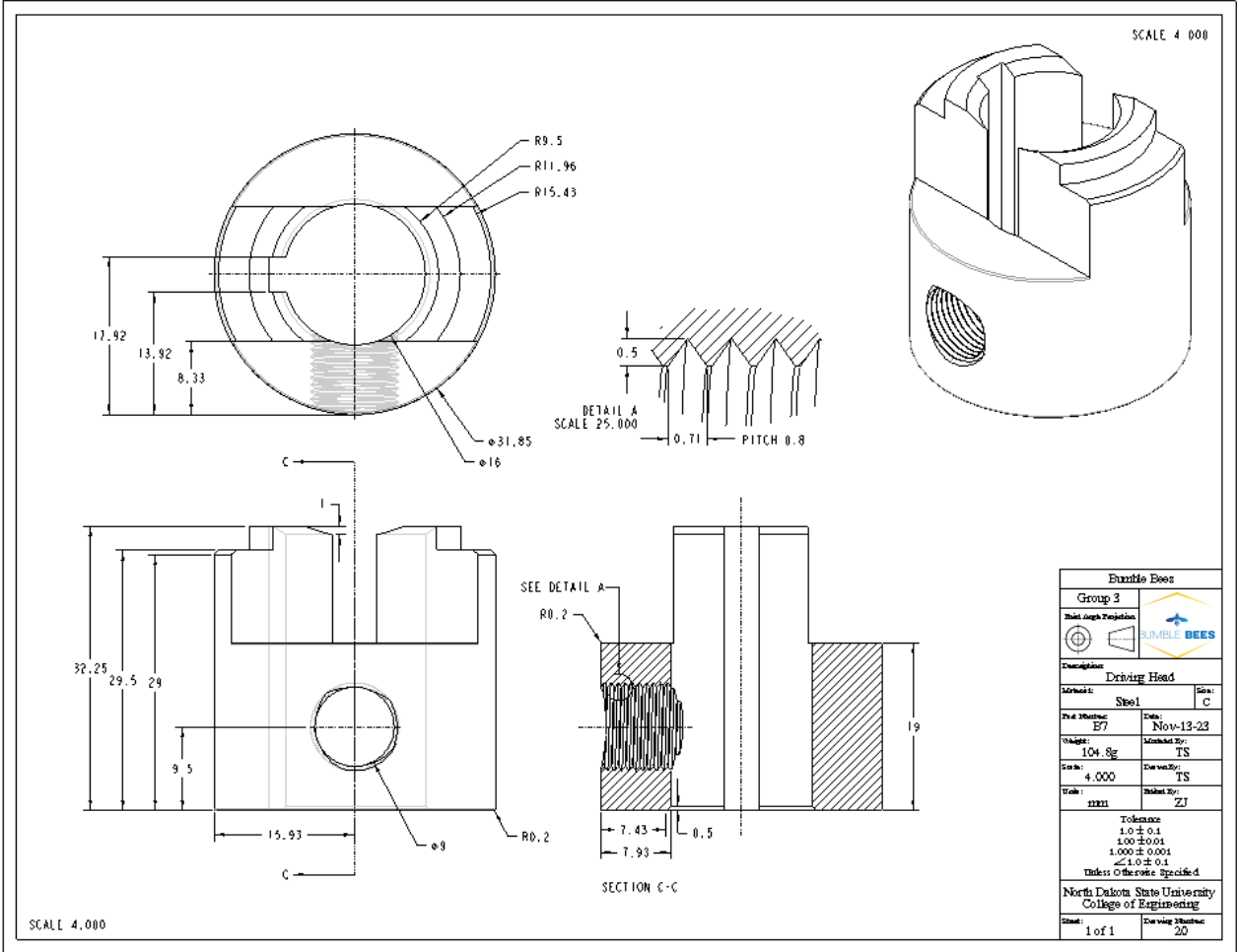
Bumble Bee	
Group 3	
	
Description: Arma tape Insulation Sheet Extr	
Location:	C
Part Number:	E18
Date:	Dec-06-23
Weight:	25.0g
Material:	TS
Size:	3.500
Drawn By:	TS
Unit:	mm
Checked By:	ZJ
Tolerances: 1.0 ± 0.1 1.00 ± 0.01 1.000 ± 0.001 ∠ 1.0 ± 0.1 Unless Otherwise Specified	
North Dakota State University College of Engineering	
Sheet:	1 of 1
Drawing Number:	E18



SECTION A-A
SCALE 3.500

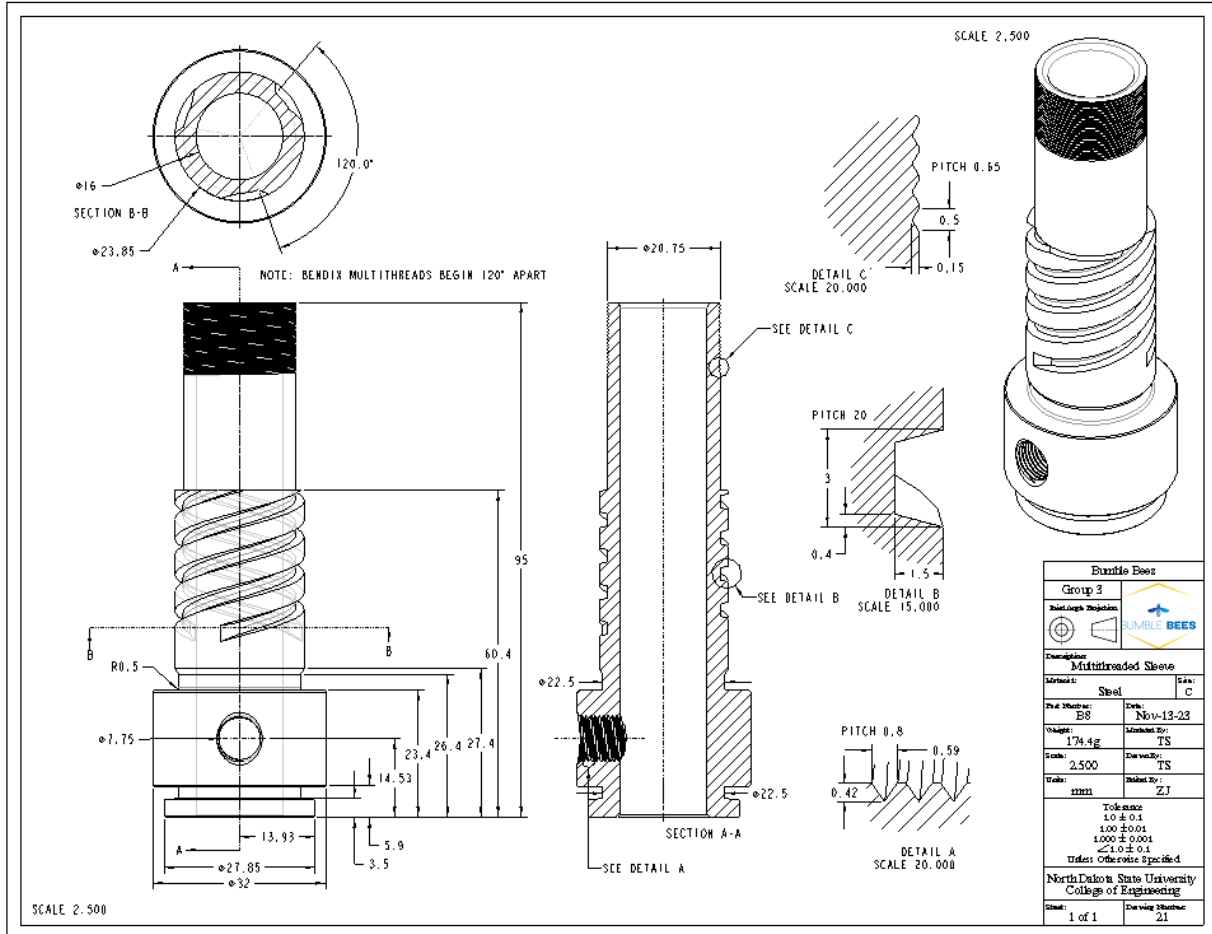






Bumble Bees	
Group 3	
	
Description: Sleeve Washer	
Material: Steel	Size: C
Part Number: ES	Date: Nov-14-23
Weight: 136.7g	Checked By: TS
Scale: 3.000	Drawn By: TS
Title: 2221	Revised By: ZJ
Tolerances: 1.0 ± 0.1 1.00 ± 0.01 1.000 ± 0.001 <math>< 1.0 \pm 0.1</math> Unless Otherwise Specified	
North Dakota State University College of Engineering	
Sheet: 1 of 1	Drawing Number: 18

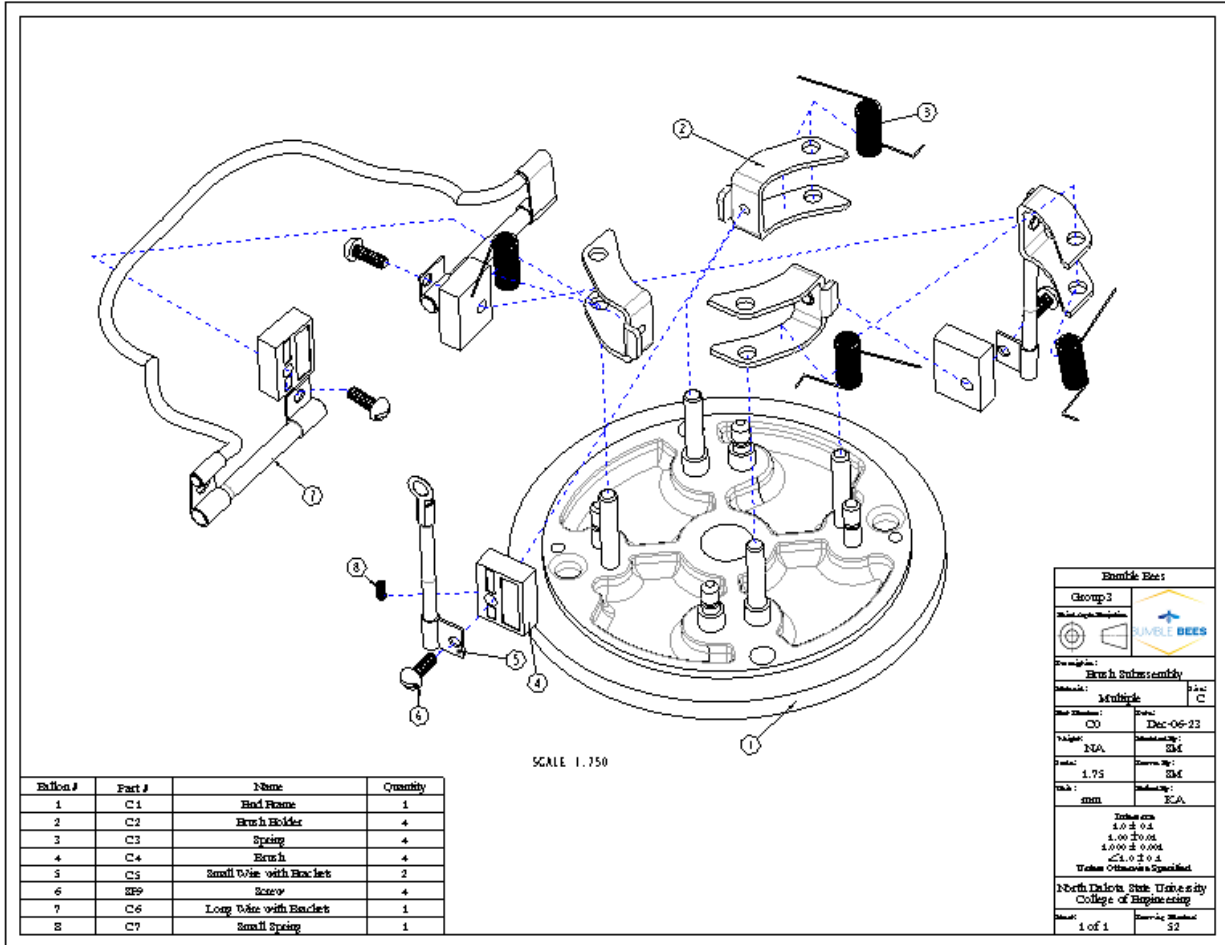


Bumble Bees	
Group 3	
	
Description: Driving Head	
Material: Steel	Size: C
Part Number: E7	Date: Nov-13-23
Weight: 104.8g	Manufact By: TS
Scale: 4.000	Drawn By: TS
Trak: xxxx	Checked By: ZJ
Tolerance 1.0 ± 0.1 1.00 ± 0.01 1.000 ± 0.001 < 1.0 ± 0.1 Unless otherwise specified	
North Dakota State University College of Engineering	
Sheet: 1 of 1	Drawing Number: 20




Buzink Beez	
Group 3	
	
Description: Multitreaded Sleeve	
Material: Steel	Case: C
Part Number: ES	Date: Nov-13-23
Weight: 174.4g	Material: TS
Scale: 2,500	Drawn By: TS
Units: mm	Checked By: ZJ
Tolerance: 1.0 ± 0.1	
1.00 ± 0.01	
1.000 ± 0.001	
1.0 ± 0.1	
Unless Otherwise Specified	
North Dakota State University College of Engineering	
Sheet: 1 of 1	Drawing Number: 21

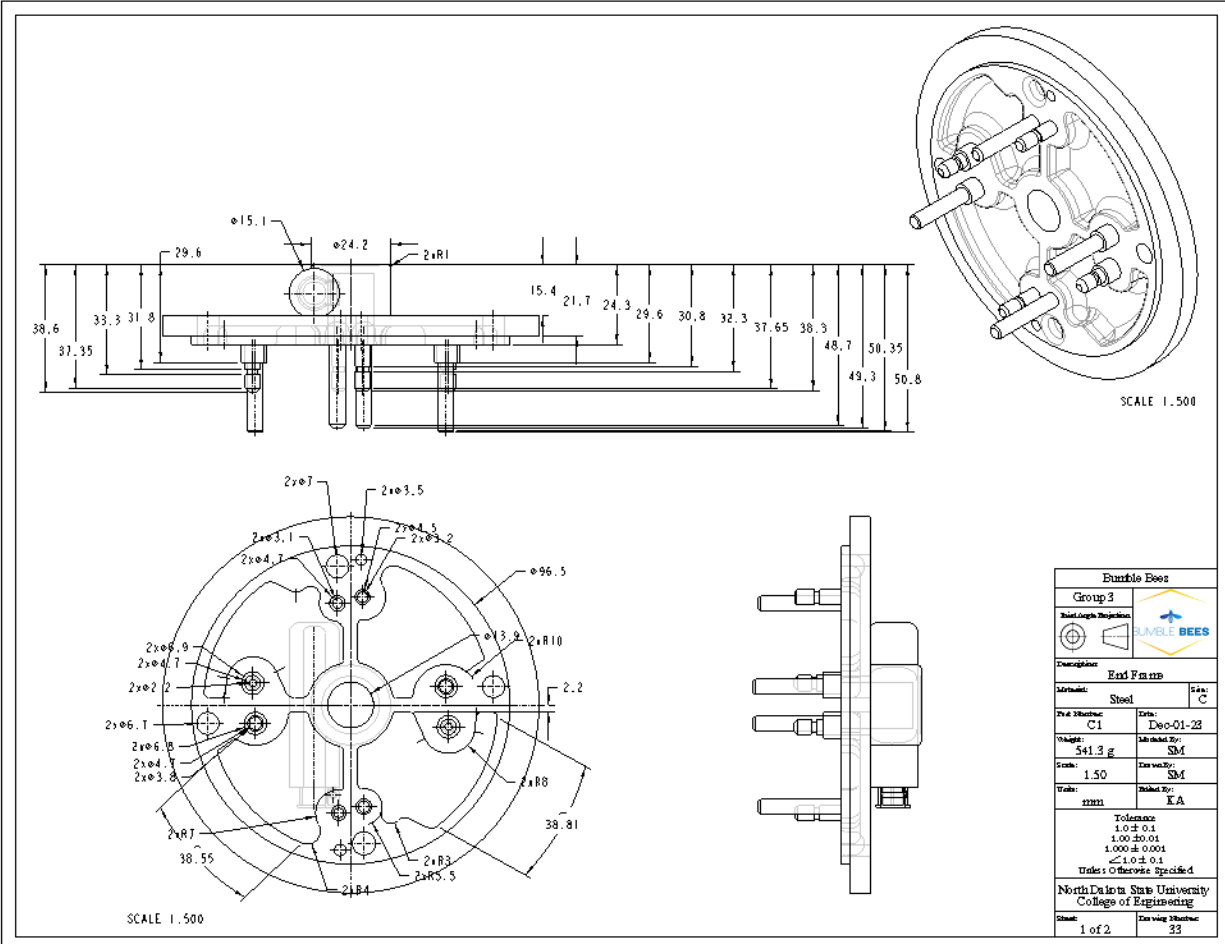
[C] BRUSHES SUBASSEMBLY



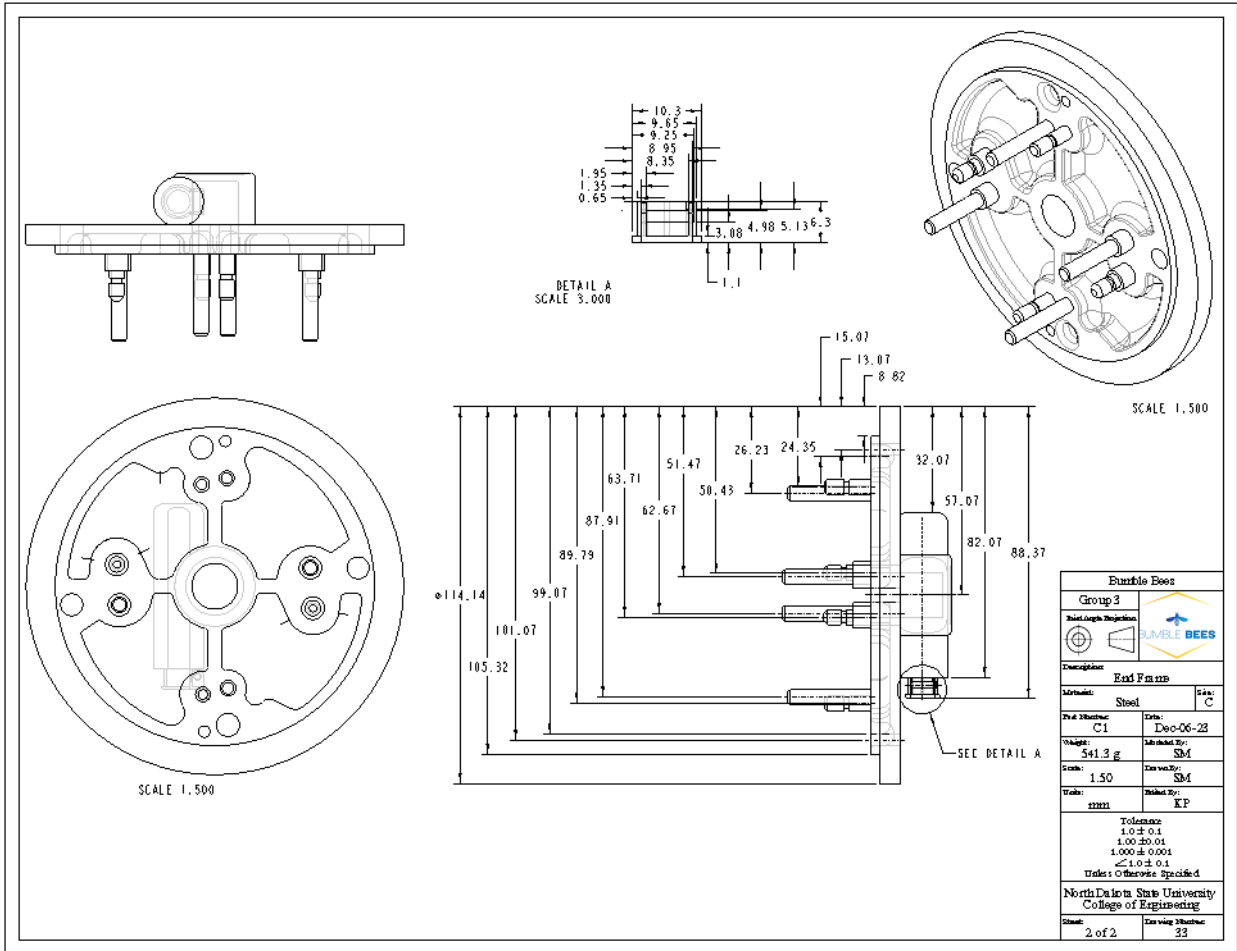
Block#	Part #	Name	Quantity
1	C1	End Frame	1
2	C2	Brush Holder	4
3	C3	Spring	4
4	C4	Brush	4
5	C5	Small Wire with Bracket	2
6	SEP	ScREW	4
7	C6	Long Wire with Basket	1
8	C7	Small Spring	1

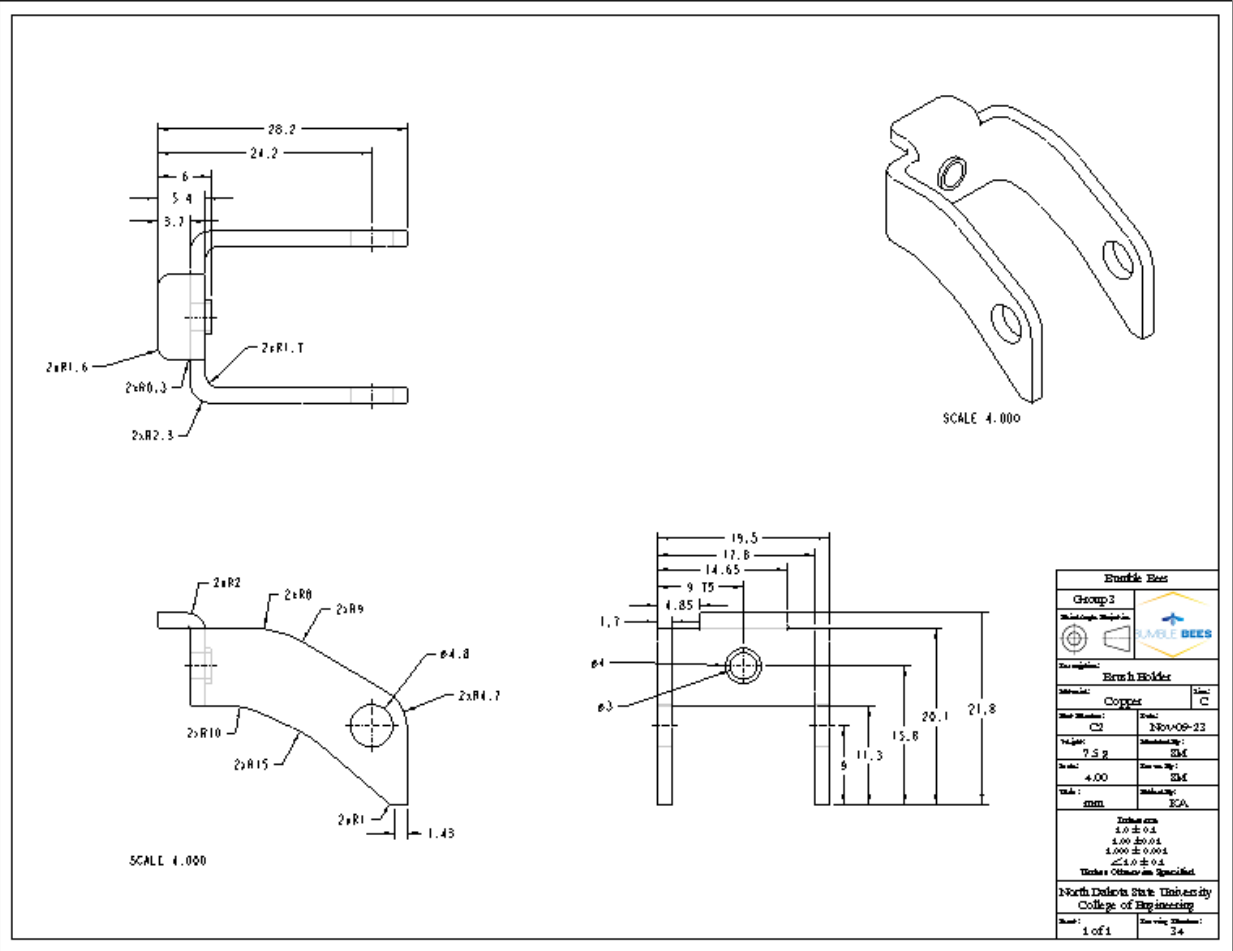
Dunkle Beer	
Group 3	
	
Part Name: Brush Subassembly	
Material: Multiple	
Part Number: CO	Rev: DEC-06-23
Weight: N/A	Manufacturer: SM
Cost: 1.75	Source No: SM
Unit: mm	Industry: ECA
Tolerances: 1.0 ± 0.1 1.00 ± 0.01 1.000 ± 0.001 0.1 ± 0.01 Unless Otherwise Specified	
North Dakota State University College of Engineering	
Sheet: 1 of 1	Sheet Number: 82

[C] ASSEMBLY DRAWINGS

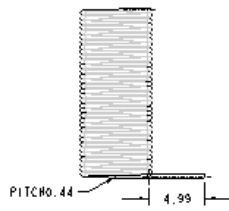
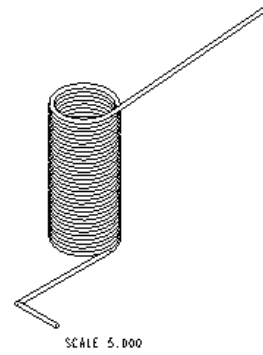
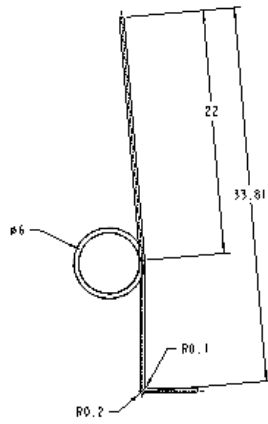


Frankie Bees	
Group 3	
Third Angle Projection	
Description: End Flange	
Material: Steel	Unit: C
Part Number: C1	Date: Dec-01-23
Weight: 541.3 g	Manufactured By: SM
Scale: 1.50	Drawn By: SM
Units: mm	Checked By: EA
Tolerances: 1.0 ± 0.1 1.00 ± 0.01 1.000 ± 0.001 Unless Otherwise Specified	
North Dakota State University College of Engineering	
Sheet: 1 of 2	Engineering Student: 33

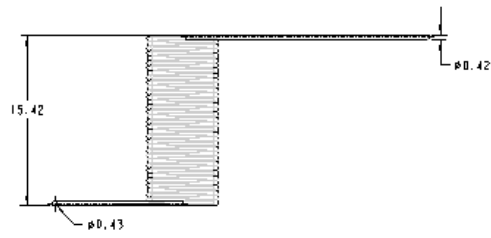




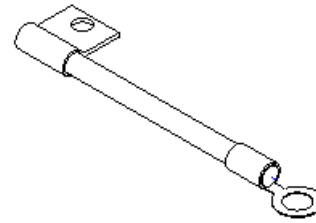
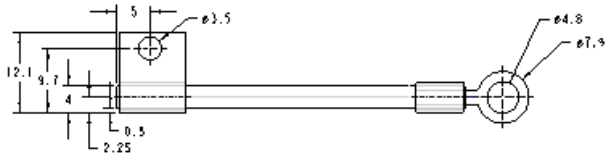
Brush Holder	
Group 2	
Part Name:	Brush Holder
Material:	Copper
Drawing Number:	230109-22
Date:	7.5.2
Scale:	4.00
Unit:	mm
Drawing Standard:	ECA
Tolerances: 1.0 ± 0.1 0.50 ± 0.04 0.00 ± 0.004 $\le 1.0 \pm 0.1$	
Manufacturer: North Dakota State University College of Engineering	
Sheet:	1 of 1
Drawing Number:	24



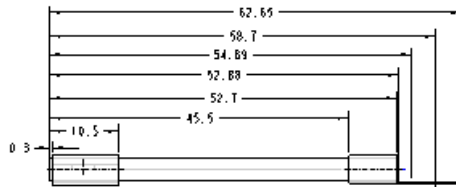
SCALE 5.000



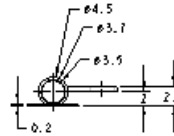
Bumble Bees		
Group 3		
Description: Spring		
Material: Steel	Size: C	
Part Name: C3	Date: Nov-14-23	
Weight: 2.70 g	Manufacturer: SM	
Scale: 5.00	Drawn By: SM	
Units: mm	Checked By: ZJ	
Tolerances: 1.0 ± 0.1 1.00 ± 0.01 1.000 ± 0.001 < 1.0 ± 0.1 Unless Otherwise Specified		
North Dakota State University College of Engineering		
Sheet: 1 of 1	Drawing Number: 35	



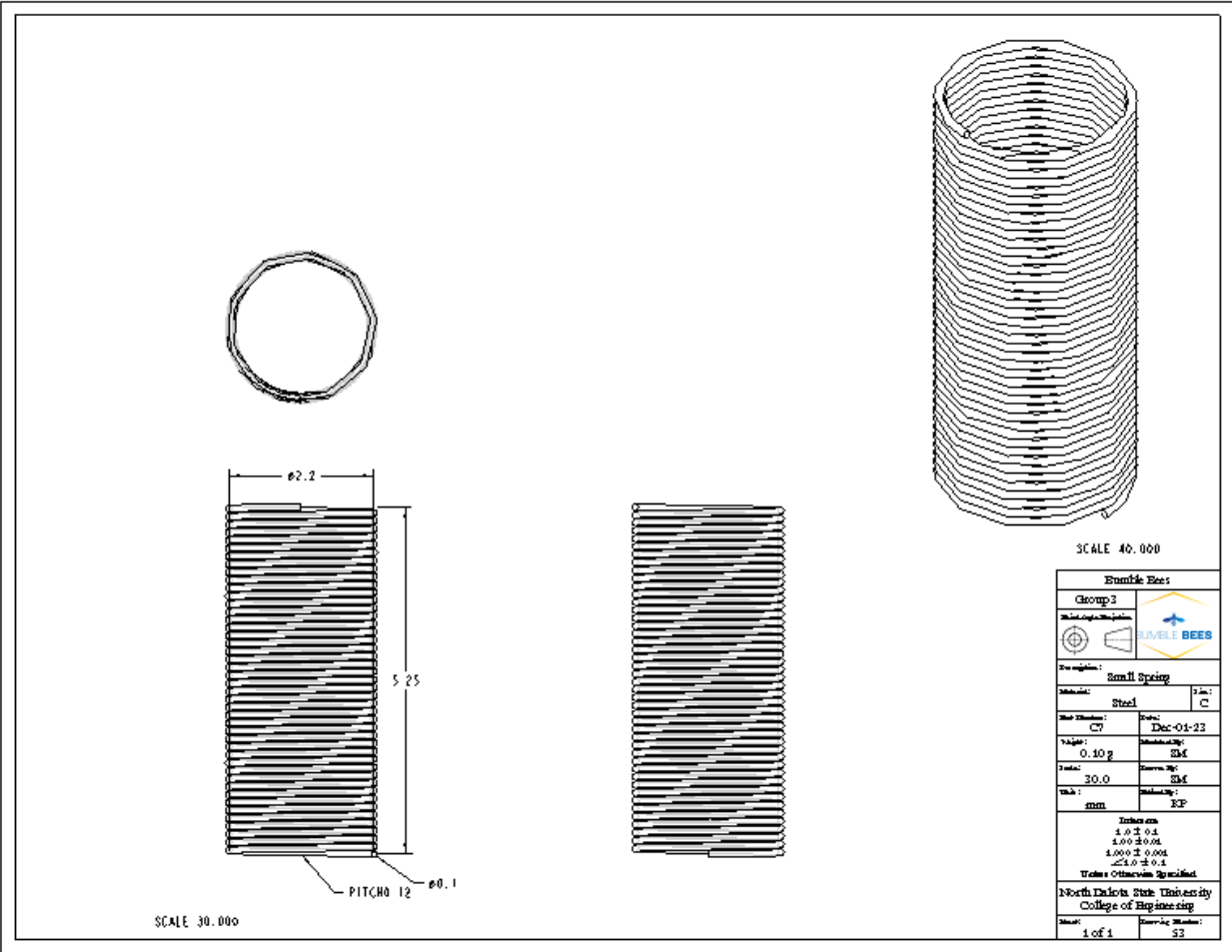
SCALE 3.000

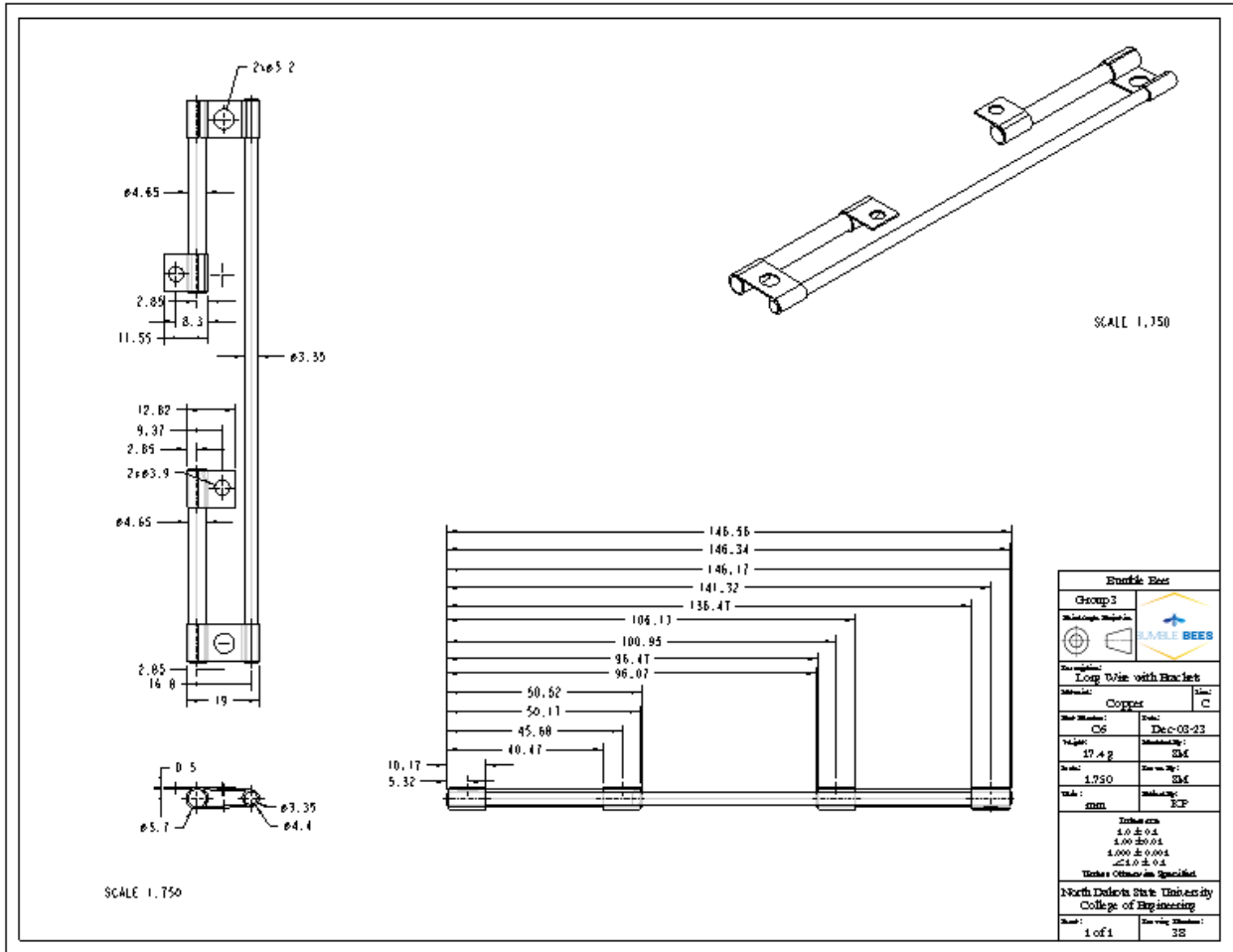


SCALE 3.000

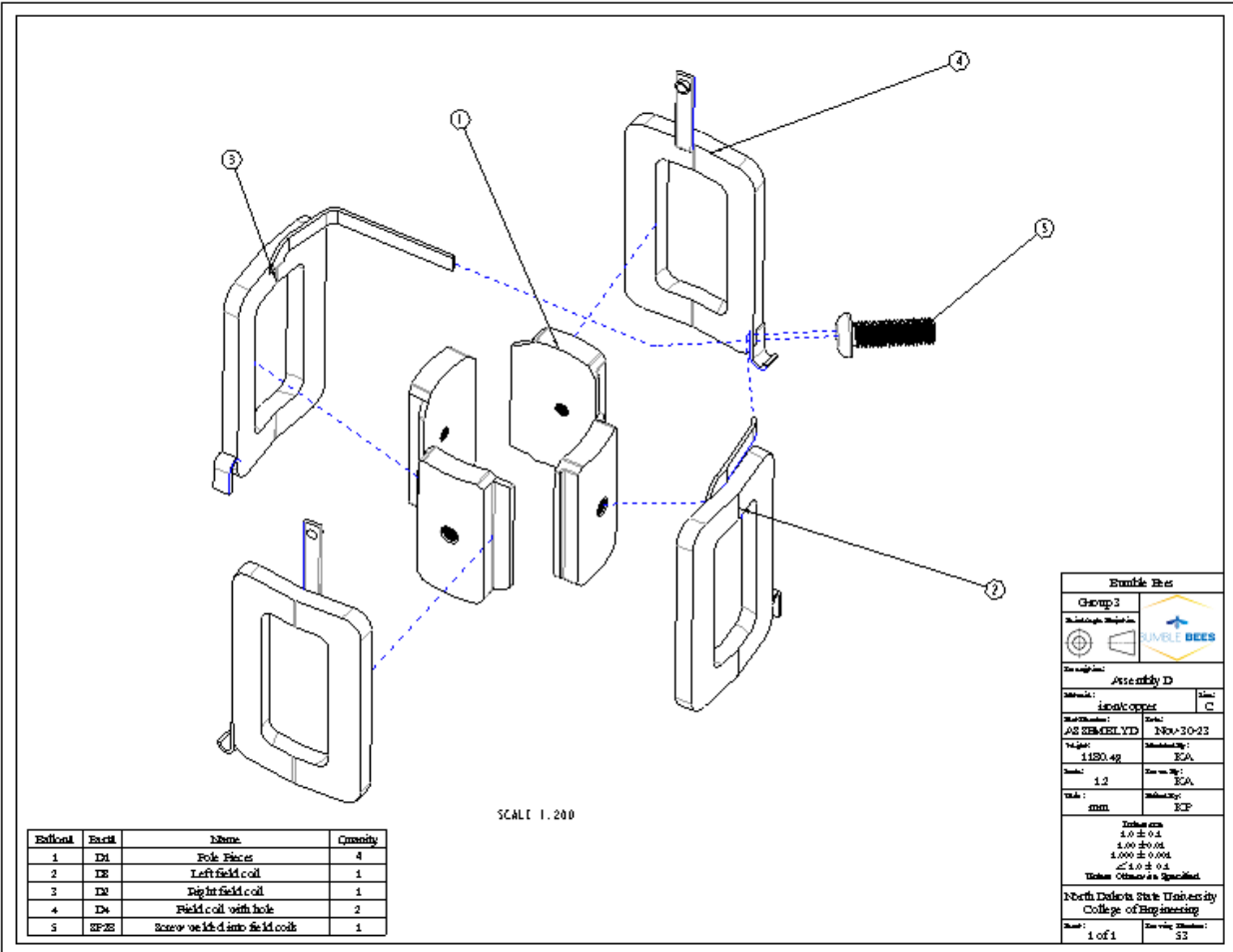


Bumble Bees	
Group 2	
Student Organization	
Project:	Short Drive & Bracket
Material:	Copper/Steel
Sheet Number:	CS
Page:	1201-11-23
Weight:	5.6 g
Cost:	3.0
Unit:	mm
Industry:	ECA
Tolerances: 3.0 ± 0.4 1.00 ± 0.04 1.000 ± 0.004 0.1 ± 0.04 Unless Otherwise Specified	
North Dakota State University College of Engineering	
Sheet:	1 of 1
Sheet Number:	37

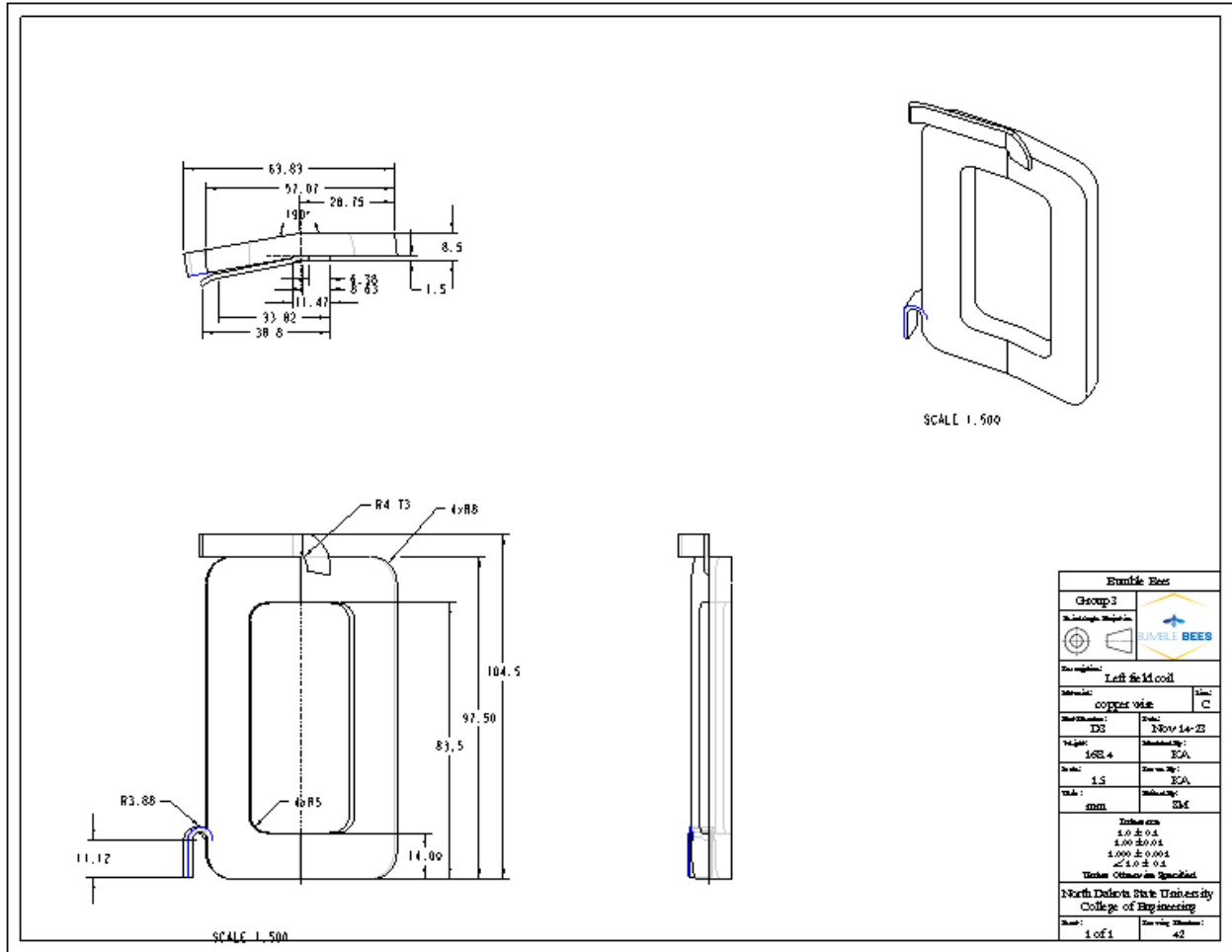


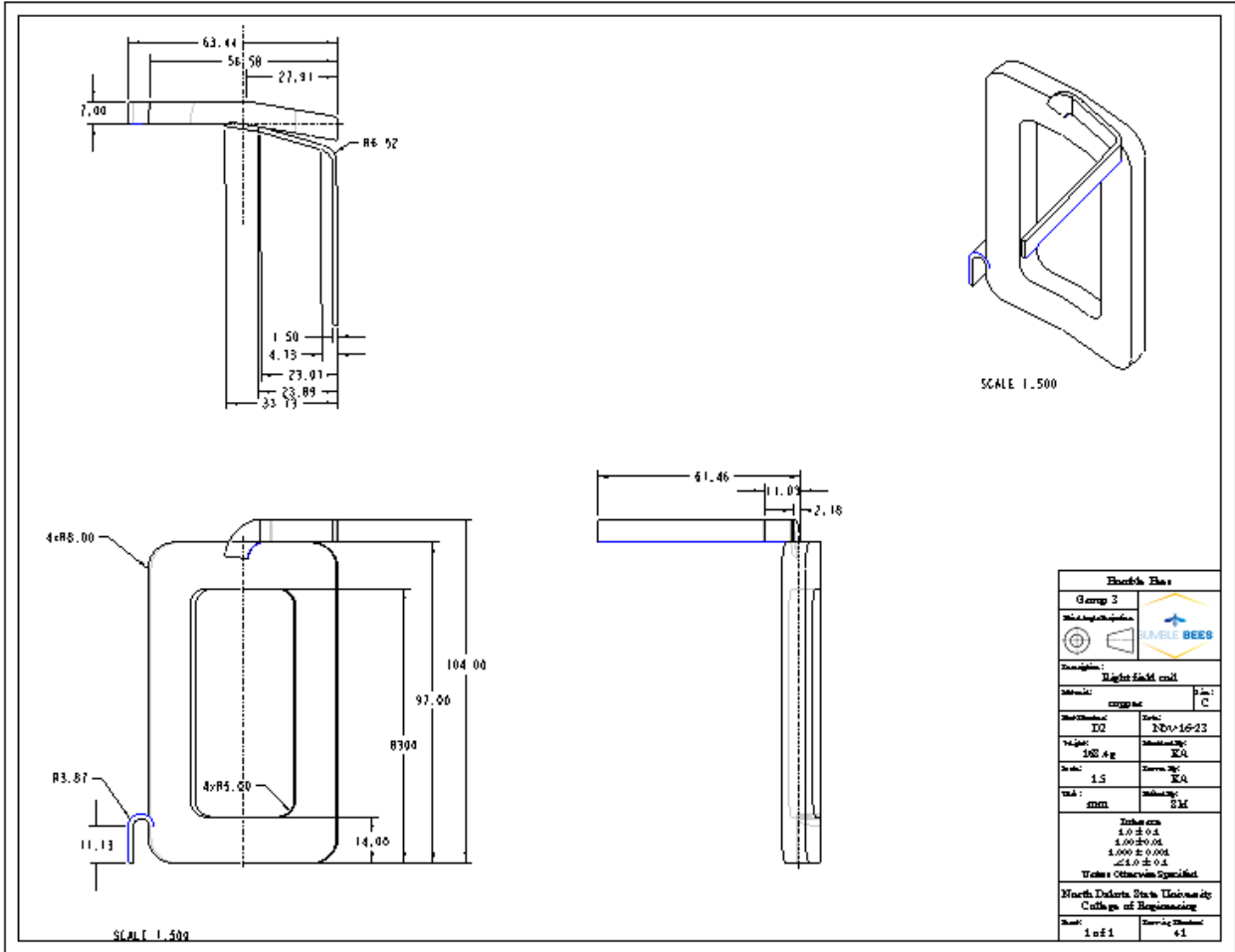


[D] FIELDS SUBASSEMBLY

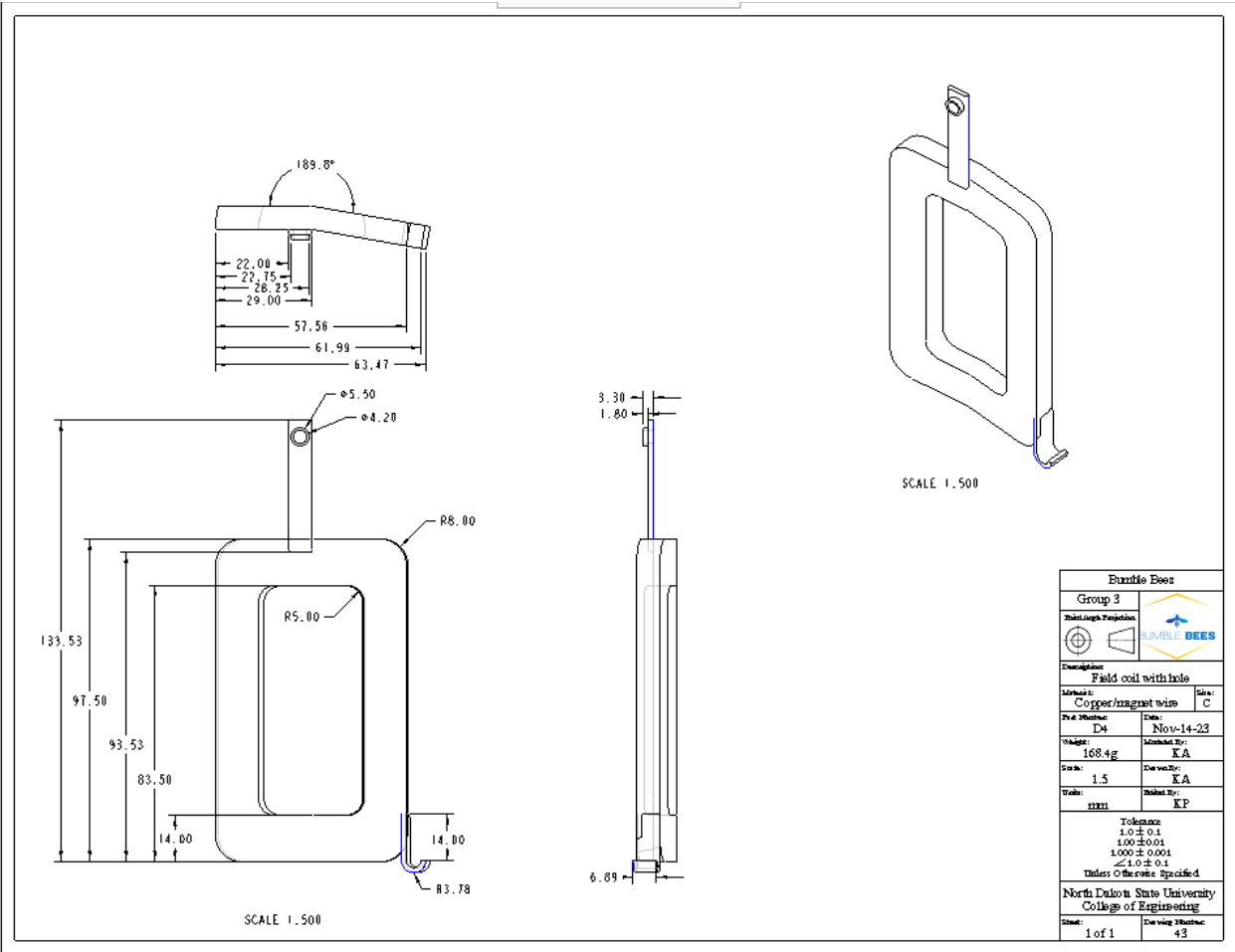


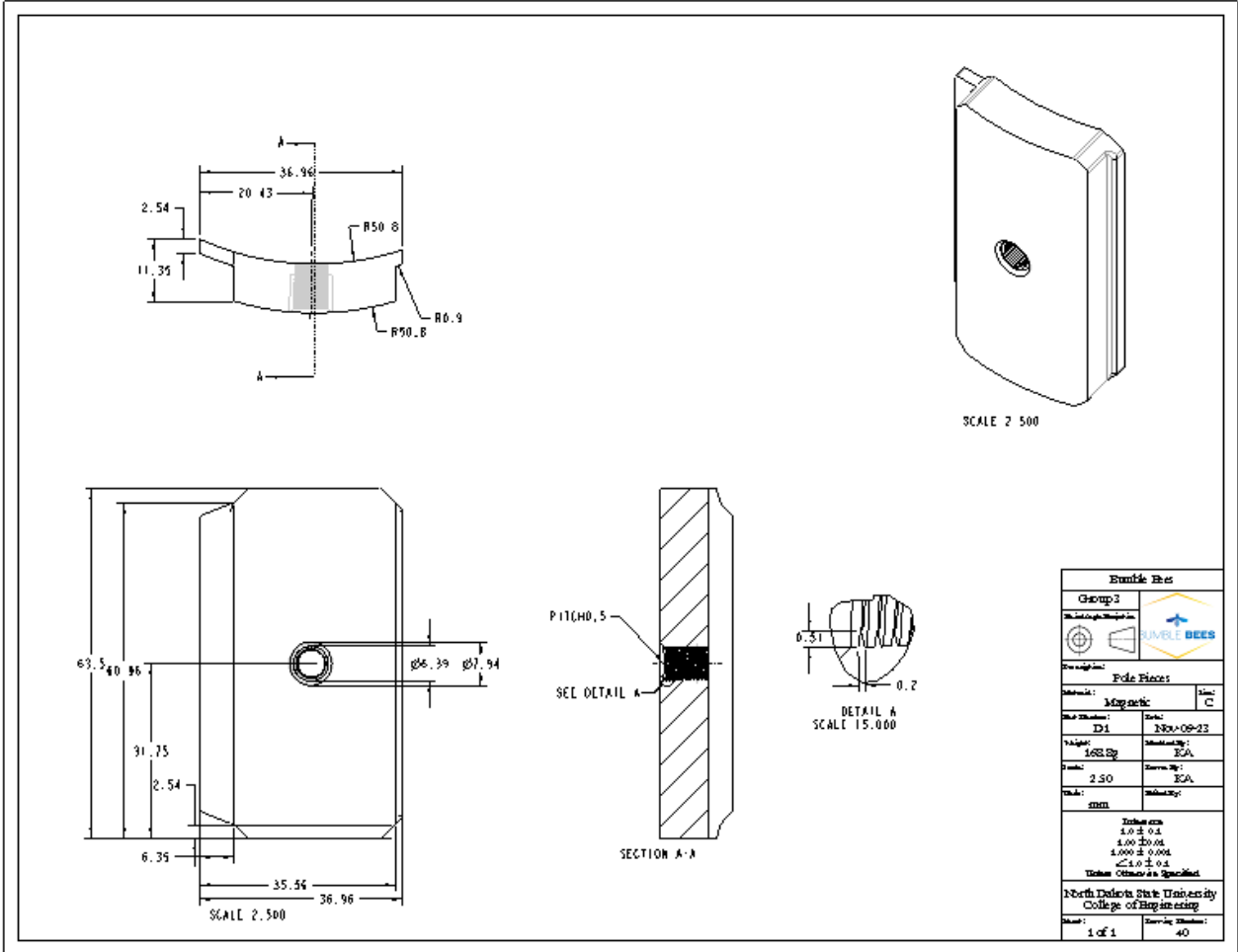
[D] ASSEMBLY DRAWINGS





Hand's On	
Group 3	
Description: Wright Field rail	
Material: aluminum	Unit: C
Part Number: 02	Date: 08/16/23
Weight: 582.4 g	Submitted By: EA
Scale: 1:5	Drawn By: EA
Unit: mm	Submitted By: SM
Tolerances: Finish: $±0.05$ Form: $±0.05$ Position: $±0.0004$ Profile: $±0.05$	
Notes: Otherwise Specified	
North Dakota State University College of Engineering	
Sheet: 1 of 1	Drawing Number: 41



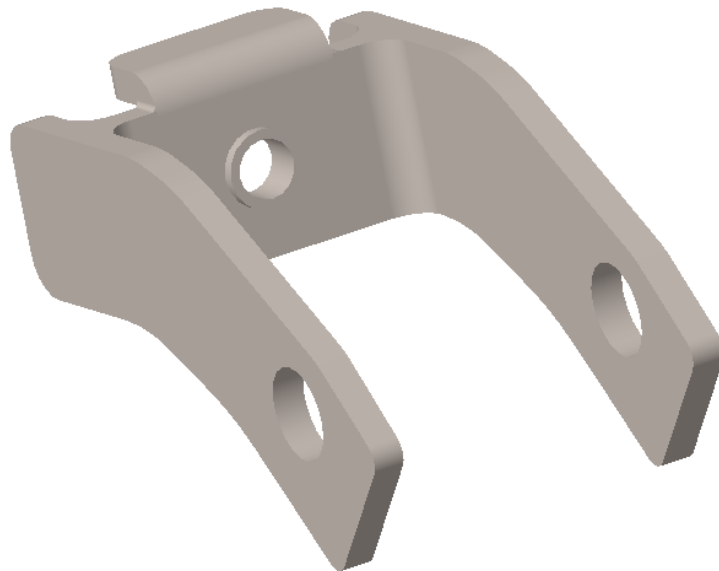


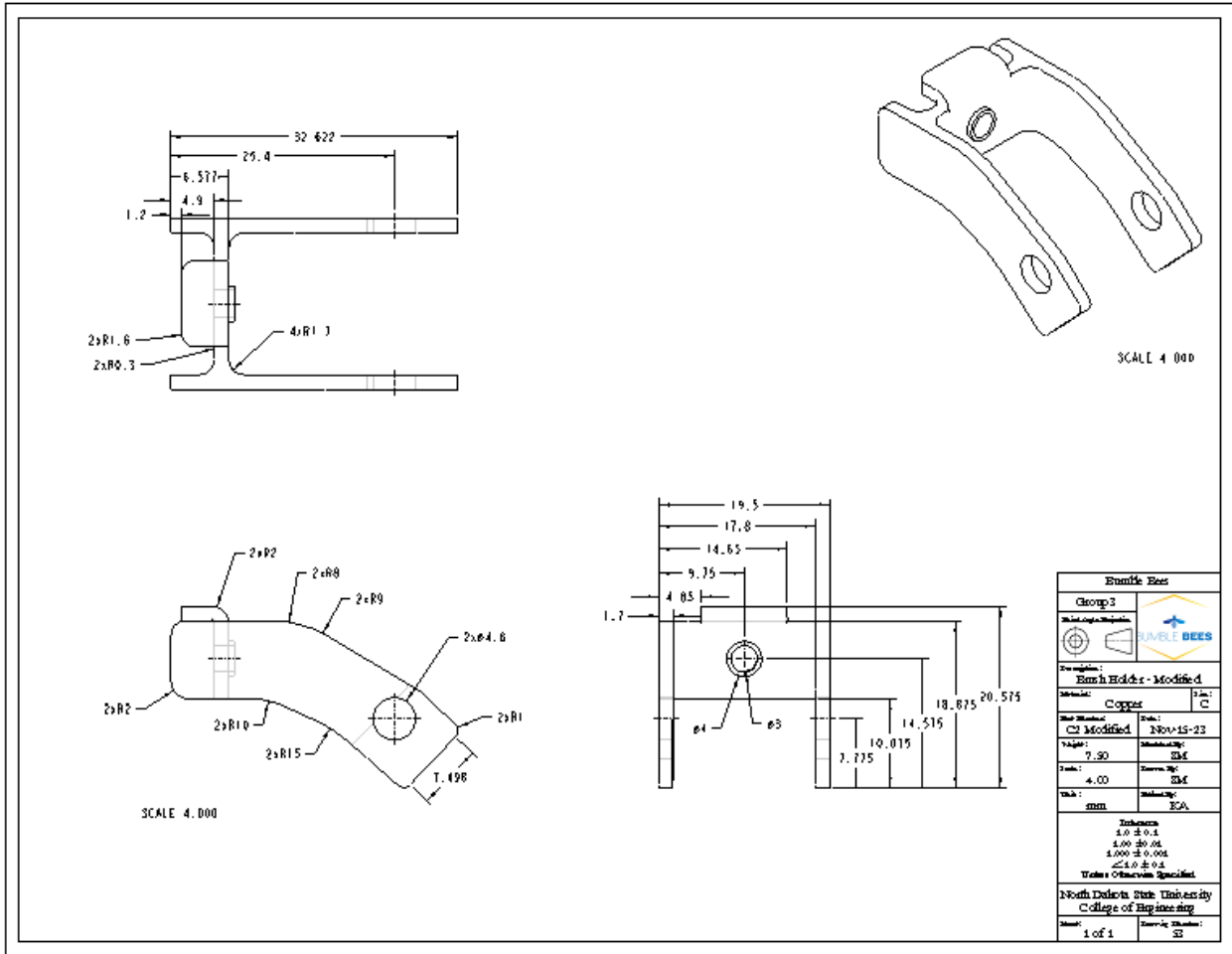
Examle Etes Group 3 	
File Places Student: Mogharib Seat: C Roll Number: D1 Date: Nov-09-23 Subject: 1682 Sp Instructor: ECA Term: 2.50 Reviewer: ECA Unit: mm Unit/Type:	
Tolerance mm 1.0 ± 0.1 0.50 ± 0.05 1.000 ± 0.004 < 1.0 ± 0.1 Unless Otherwise Specified	
North Dakota State University College of Engineering	
Sheet: 1 of 1	Drawing Number: 40

MODIFICATION & DESIGN CHANGE

[1] BRUSH HOLDER

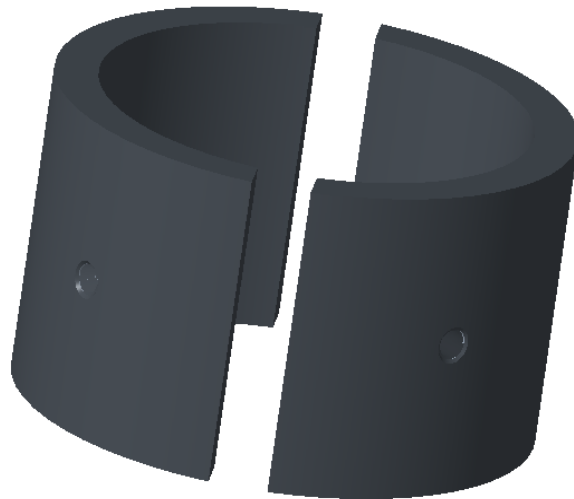
I picked the brush holder to be the part that I modified. I chose this part because I thought a few simple modifications would improve the stability of the part. The first modification that I added was two extra plates on the front of the brush holder. The point of this is to keep the brush in a more stable position and to keep it from moving. The second modification I made was taking both sides of the brush holder and extending them and making them squared off instead of rounded. I did this because there is a spring that sits in between the two sides. With the ends of the holder being rounded, some of the springs will stick out. Now that they are squared off, the spring will fit more comfortably inside of the brush holder. It also will help protect the spring.

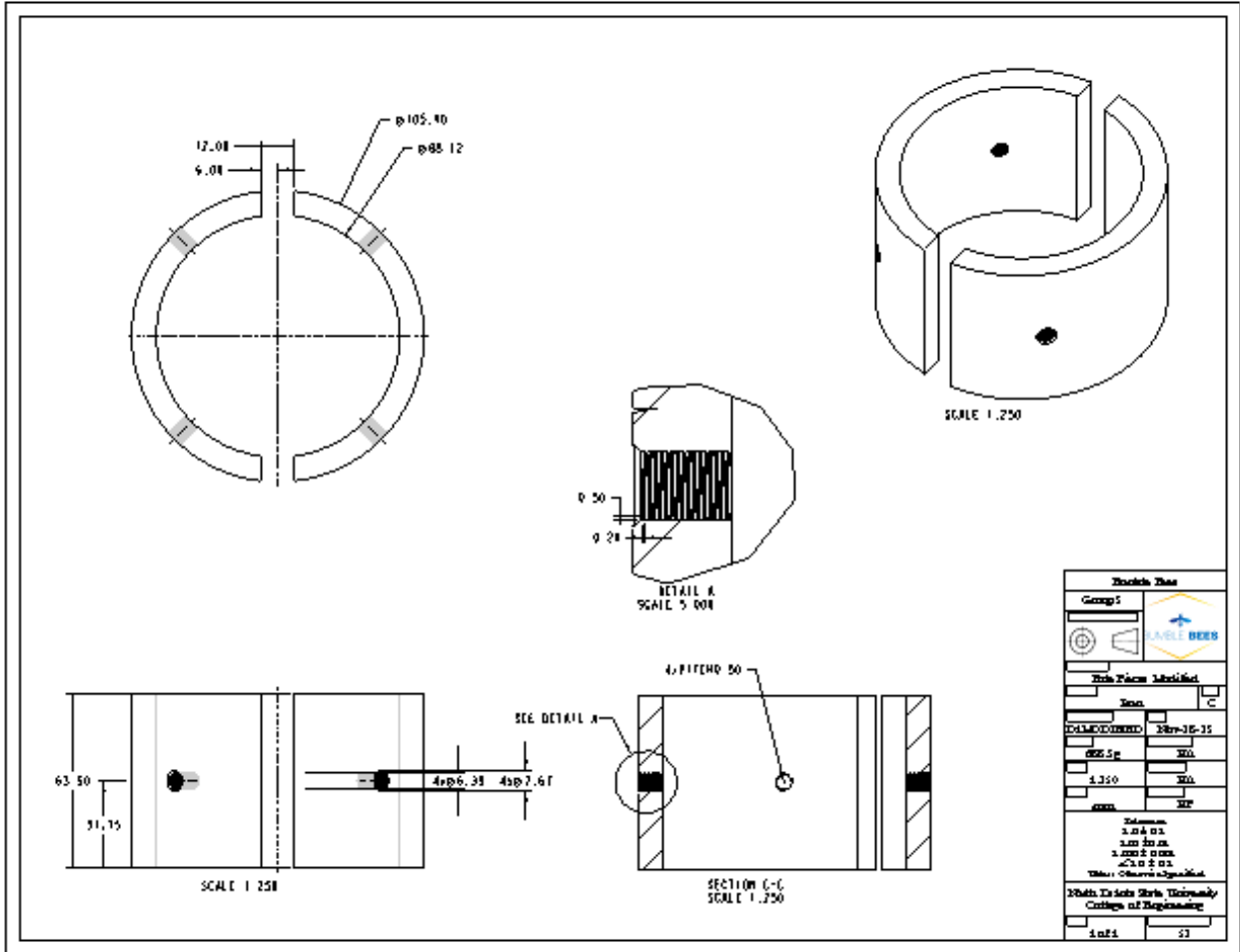




[II] MAGNETIC FIELDS

I decided to modify the pole pieces and field coils. I did some research and found that it is more efficient to have a magnet around the entire inside of the drive housing. I decided on this modification because it is a simpler structure, gives higher power, and is more cost-effective. Having a magnet around the whole inside causes the armature to spin faster, increasing the torque. This also reduces the amount of parts inside the starter motor. The start motor would be lighter in weight and easier to move around. I believe that having solid magnets on the inside would create a better and more efficient start for our motor.

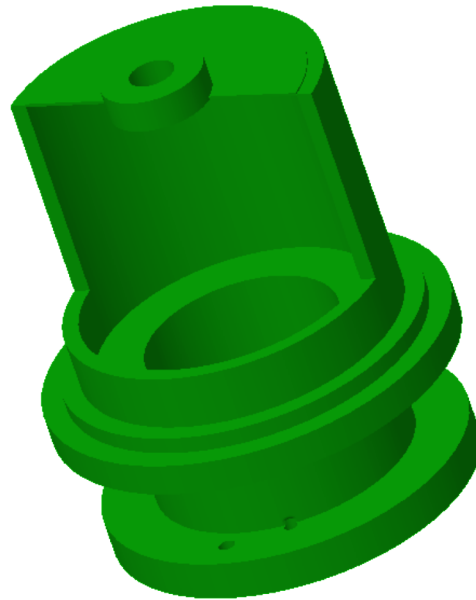


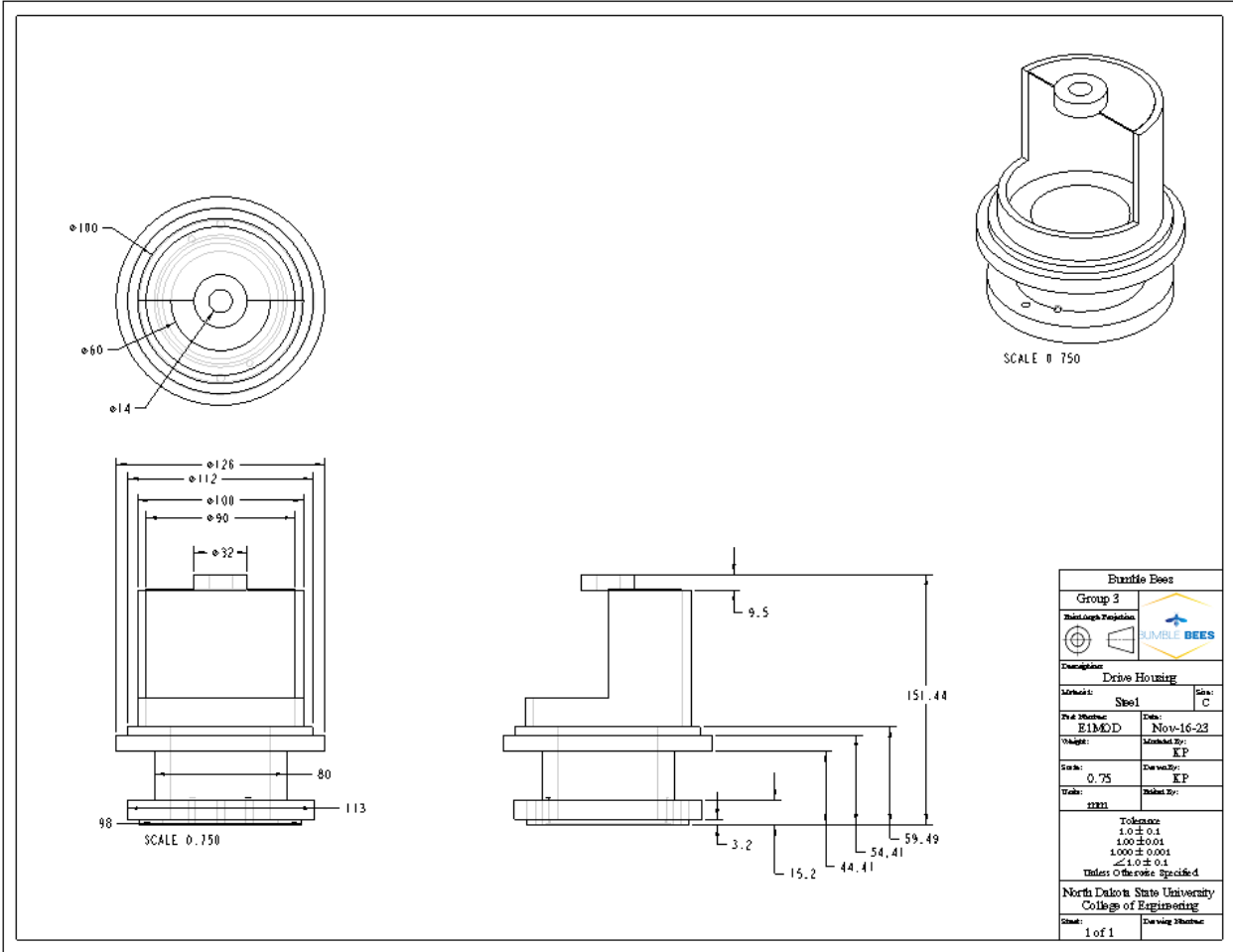


Escriba Here	
Grupo 1	
Este Plano Identificado	
Escala	
ELABORADO	Rev-16-15
600.5g	300
4.350	300
3000	300
Dimensiones: 1.00 0.2 1.00 0.25 1.00 0.3 1.00 0.4 1.00 0.5	
Dibujado En AutoCAD, Verificado Oficina de Ingeniería	
4x4	33

[III] DRIVE HOUSING

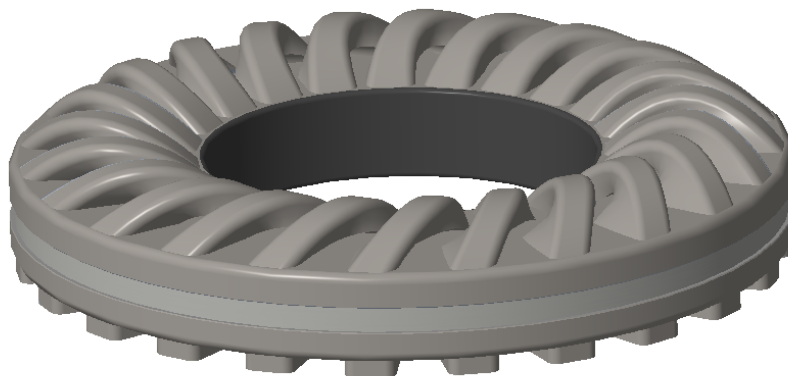
I altered the design of the drive housing, and after thorough research, I have determined that a simplified, cylindrical shape would offer significant manufacturing advantages. This modification reduces the intricacy of the component, making it more straightforward to produce. The cylindrical form facilitates seamless installation and diminishes the number of required screws to maintain structural integrity. By opting for this streamlined shape, the manufacturing process becomes more efficient, while the ease of assembly enhances the overall functionality of the part, making me believe this would be beneficial for our project.

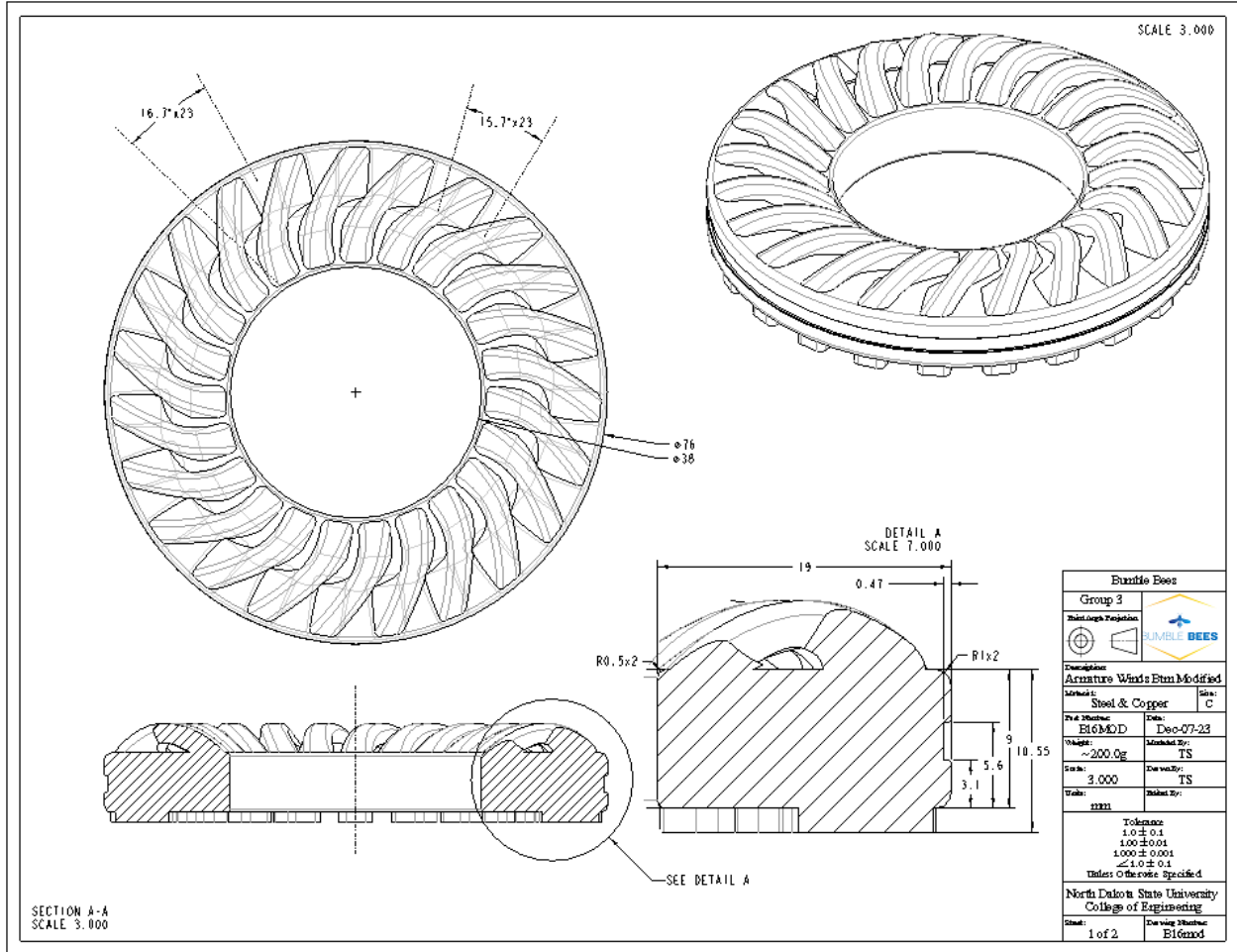


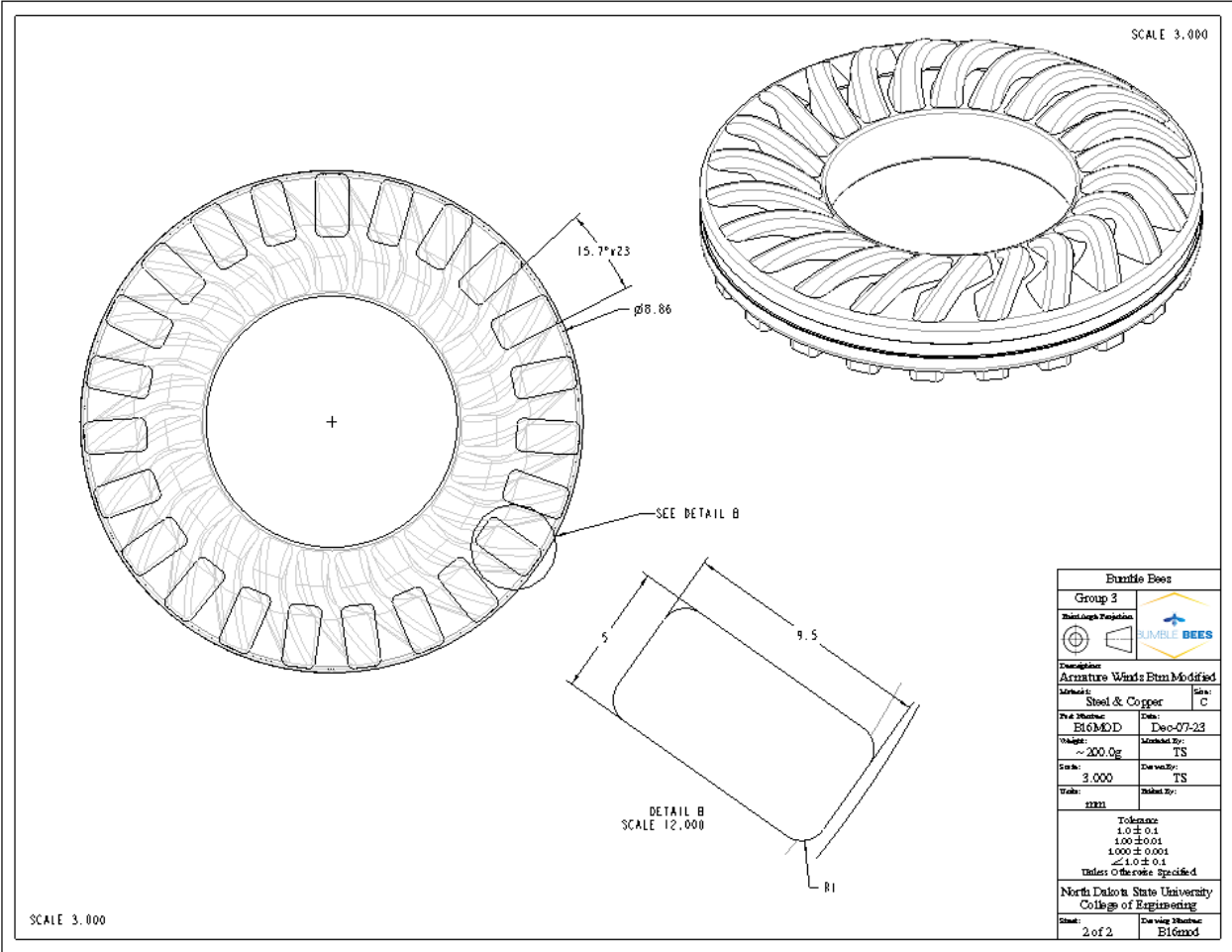


[IV] BOTTOM ARMATURE COILS

I altered the winds of the armature coils. In its present configuration, it is difficult to maintain if ever needing maintenance and may be subject to unwanted forces when manufacturing. Upon inspection, it became apparent that the winds were made straight then bent at a later point to create the winds. This modification would add a large solid bar between the winds to reduce the stress at the points of shear during the manufacturing of the winds and would reduce the need for insulation at the top of the commutator. This also simplifies the part by reducing the extra "twist" the winds need during manufacturing while reducing the chances of the material to break.









SCALE 3.000

15.7 ± 0.23
 Ø8.86

SEE DETAIL B

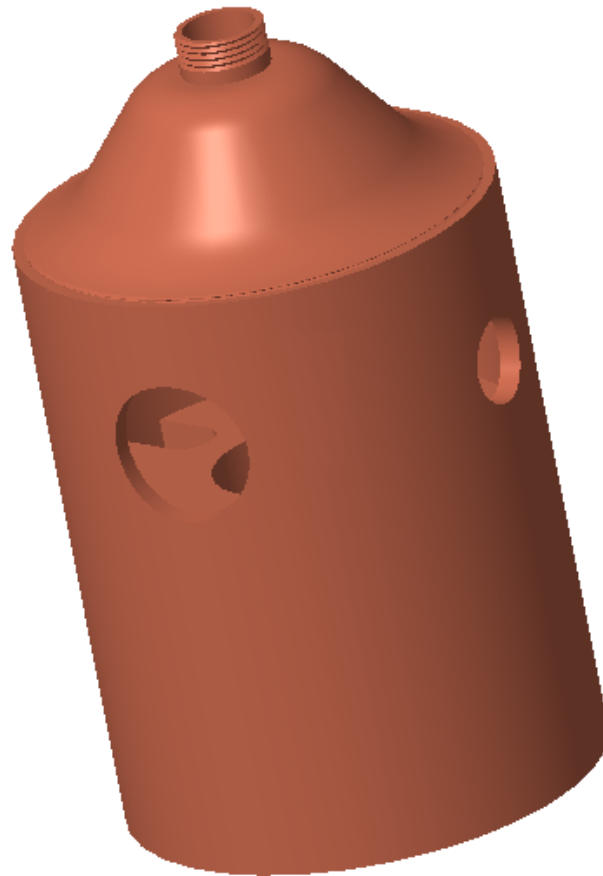
DETAIL B
 SCALE 12.000

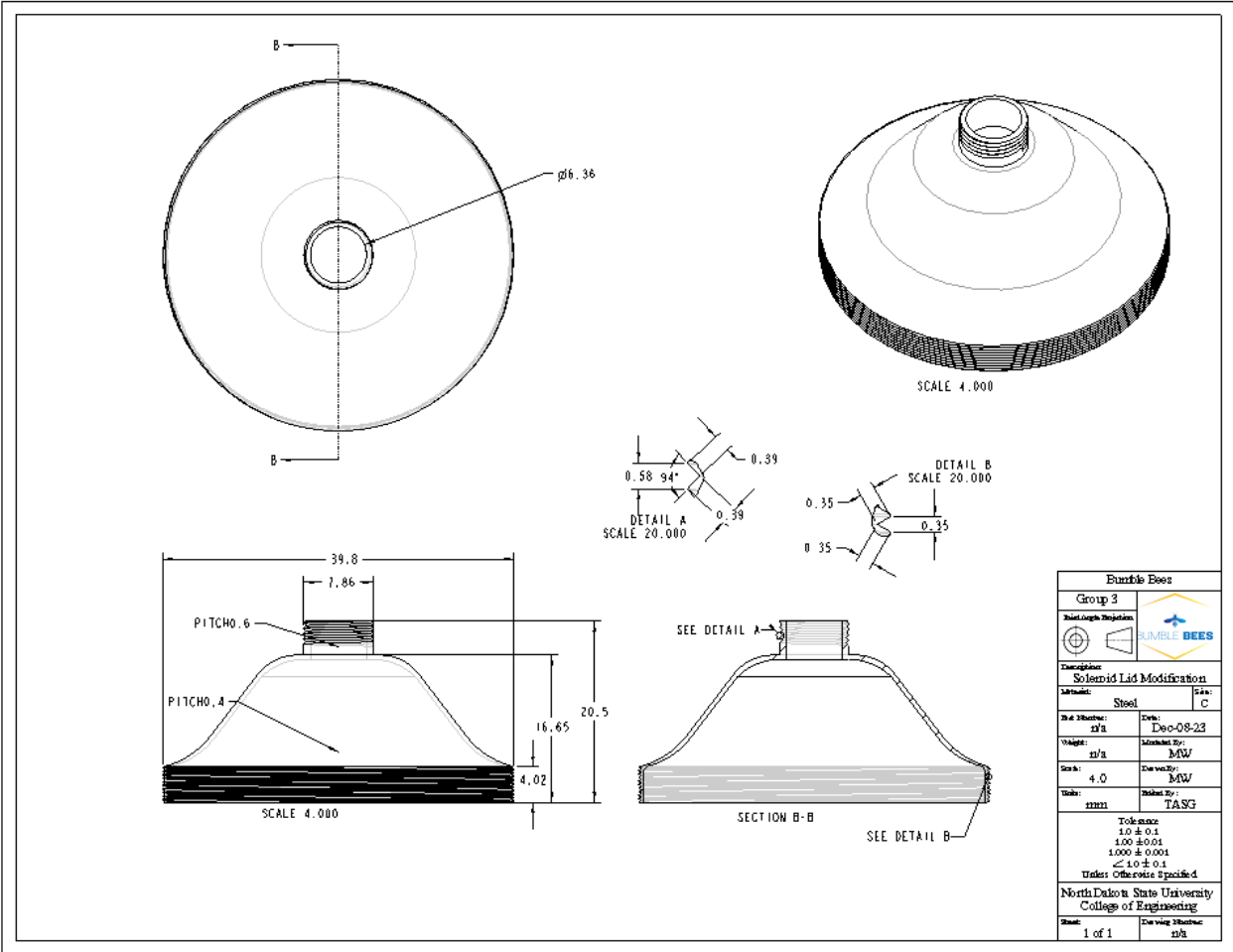
SCALE 3.000

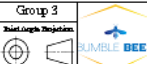
Bumble Bees	
Group 3	
 Bumble Bees	
Description: Armature Winding Modified	
Material: Steel & Copper	Case: C
Part Number: B16MOD	Date: Dec-07-23
Weight: ~200.0g	Manufactured By: TS
Scale: 3.000	Drawn By: TS
Works: 22221	Sheet No:
Tolerance: 1.0 ± 0.1 1.00 ± 0.01 1.000 ± 0.001 < 1.0 ± 0.1 Unless Otherwise Specified	
North Dakota State University College of Engineering	
Sheet: 2 of 2	Drawing Number: B16MOD

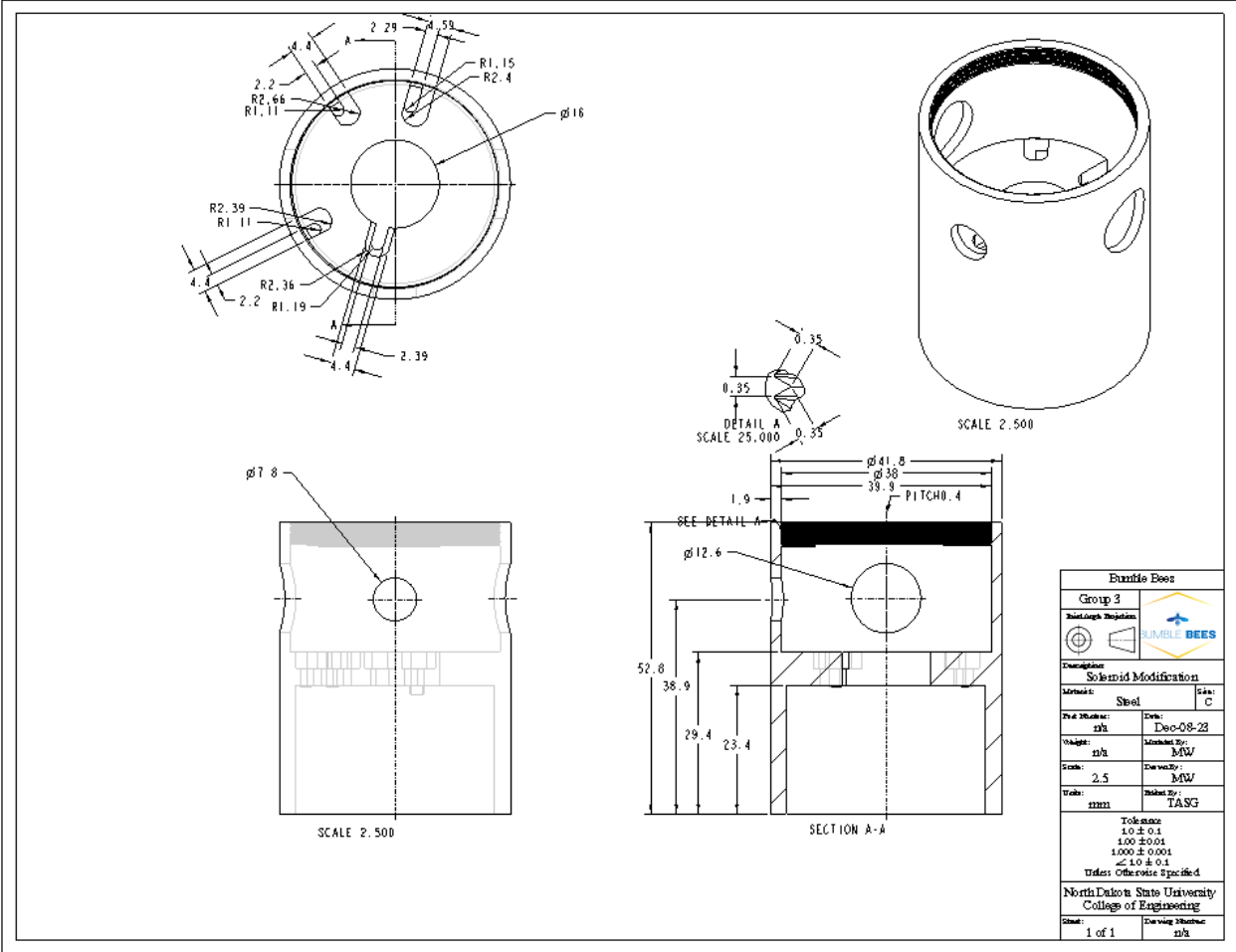
[V] SOLENOID

One of the first main issues our group ran into was the disassembly of the solenoid. The cap was press-fit into the main body of the solenoid with excess steel being bent over the top edge to hold it in place. In order to get access to the inside of the part, we had to cut it open. This modification is making the disassembly and access to the inside of the solenoid much easier. I have decided to extend the bottom of the cap 4 millimeters straight down in order to put threads on that wall, and on the wall of the solenoid body. With access to the inside of the solenoid now being held together by threads, maintenance and disassembly will be much easier.





Bumble Bees	
Group 3	
	
Description: Solenoid Lid Modification	
Material: Steel	Case: C
File Number: 22A	Date: Dec-08-23
Weight: 22/g	Minister By: MW
Size: 4.0	Drawn By: MW
Units: mm	Checked By: TASC
Tolerances: 1.0 ± 0.1 1.00 ± 0.01 1.000 ± 0.001 ≤ 1.0 ± 0.1 Unless Otherwise Specified	
North Dakota State University College of Engineering	
Sheet: 1 of 1	Drawn Sheet: 22A



[VI] TWO HOLED BRACKET

The part that was modified was part A9, the 2 holed bracket. This part was chosen to be modified because of the difficulties it caused to disassemble the solenoid. The current design of the 2 holed bracket blocks access to another bolt that is required to remove the solenoid from the rest of the starter. In order to remove these bolts our group had to use excessive force and a vice grip. This method seemed unnecessary and tedious to remove a bolt. Modifying the 2 holed bracket will make the entire solenoid easier to remove from the rest of the starter. The new design of the 2 holed bracket will include making the bracket larger and changing the placement of the bracket down. This will fix the issue of blocking access to other bolts, therefore making it easier to disassemble the solenoid.

